

# Teoria i metody optymalizacji

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# Szczególne przypadki równania Eulera

Równanie Eulera–Lagrange’a jest równaniem różniczkowym drugiego rzędu.

$$F_y - \frac{d}{dx} F_{y'} = 0$$

Funkcja podcałkowa nie zależy od  $x$ :  $F = F(y, y')$

$$F - y'F_{y'} = C$$

$$J(y) = \int_a^b F(x, y(x), y'(x)) dx$$

Dowód

$$\frac{d}{dx} (F - y'F_{y'}) = F_y y' + \underbrace{F_{y'} y'' - y'' F_{y'}}_0 - y' \frac{d}{dx} F_{y'} =$$

Funkcja złożona

$$y' \underbrace{\left( F_y - \frac{d}{dx} F_{y'} \right)}_0 = 0$$

To jest równanie różniczkowe 1 rzędu

# Przykład

$$J = \int_0^1 (y^2 + y'^2) dx$$

$$y(0) = 3$$

$$y(1) = 2$$


$$F = y^2 + y'^2$$

$$F - y'F_{y'} = C$$

$$F_{y'} = 2y'$$

$$F = y^2 + y'^2 - 2y'^2 = y^2 - y'^2 = C$$

$$y(x)^2 - y'(x)^2 = C$$

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Input:

$$y(x)^2 - y'(x)^2 = C$$

ODE classification:

first-order nonlinear ordinary differential equation

Alternate forms:

$$C + y'(x)^2 = y(x)^2$$

$$(y(x) - y'(x))(y'(x) + y(x)) = C$$

Differential equation solutions:

$$y(x) = \frac{1}{2} (C e^{x-c_1} + e^{c_1-x})$$

$$y(x) = \frac{1}{2} (C e^{-c_1-x} + e^{c_1+x})$$

# Szczególne przypadki równania Eulera

Równanie Eulera–Lagrange’a jest równaniem różniczkowym drugiego rzędu.

$$F_y - \frac{d}{dx} F_{y'} = 0$$

Funkcja podcałkowa nie zależy od  $y$ :

$$J(y) = \int_a^b F(x, \cancel{y(x)}, y'(x)) dx$$

0

$$F = F(x, y'(x))$$

$$F_y = \frac{\partial F}{\partial y}, \quad F_{y'} = \frac{\partial F}{\partial y'}$$

$$-\frac{d}{dx} F_{y'} = 0 \Rightarrow F_{y'} = C$$

To jest równanie różniczkowe 1 rzędu

# Przykład

$$J = \int_0^1 (x^2 + y'^2) dx \quad \begin{array}{l} y(0) = 3 \\ y(1) = 2 \end{array}$$



$$F = x^2 + y'^2$$

$$F_{y'} = C$$

$$F_{y'} = 2y'$$

$$2y' = C$$

$$2*y'(x)=C$$

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Input:

$$2 y'(x) = C$$

ODE names:

Separable equation

$$y'(x) 2 = C$$

Homogeneous equation

$$y'(x) = \frac{C}{2}$$

Exact equation

$$-C dx + 2 dy = 0$$

ODE classification:

first-order linear ordinary differe

Alternate form:

$$y'(x) = \frac{C}{2}$$

Differential equation solution:

$$y(x) = c_1 + \frac{C x}{2}$$

# Szczególne przypadki równania Eulera

Funkcja podcałkowa nie zależy od  $y'$ :

$$F = F(x, y)$$

$$F_y - \frac{d}{dx} F_{y'} = 0$$

$$F_{y'} = 0 \Rightarrow F_y = 0$$

To nie jest równanie różniczkowe

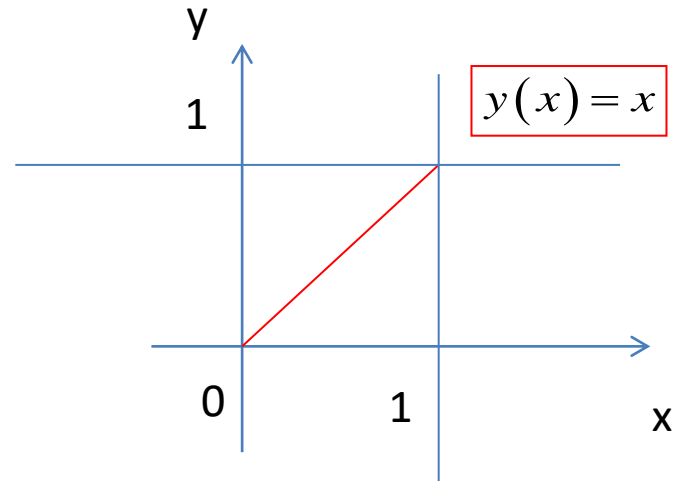
# Przykład

$$J = \int_0^1 (y - x)^2 dx \quad \begin{array}{l} y(0) = 0 \\ y(1) = 1 \end{array}$$

$$F = (y - x)^2$$

$$F_y = 2(y - x)$$

$$F_y = 0$$



$$y(x) = x$$

$$J = \int_0^1 (x - x)^2 dx = 0$$

# Szczególne przypadki równania Eulera

Funkcja podcałkowa zależy wyłącznie od  $y'$ :

$$F = F(y')$$

$$F_y - \frac{d}{dx} F_{y'} = 0$$

$$\frac{d}{dx} F_{y'} = 0 \Rightarrow F_{y'} = C \Rightarrow y(x) = C_1 x + C_2$$

$$y(x) = C_1 x + C_2$$



# Przykład

$$J = \int_0^1 (y'^2) dx \quad \begin{array}{l} y(0) = 3 \\ y(1) = 2 \end{array}$$

$$F = y'^2$$

$$\frac{d}{dx} F_{y'} = 0 \Rightarrow F_{y'} = C \Rightarrow y(x) = C_1 x + C_2$$

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$$y'(x) = C$$

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Input:

$$y'(x) = C$$

ODE names:

Separable equation

$$y'(x) = C$$

Homogeneous equation

$$y'(x) = C$$

---

Exact equation

$$-C dx + dy = 0$$

ODE classification:

first-order linear ordinary

Differential equation solution

$$y(x) = c_1 + C x$$

# Równania dla kilku funkcji

$$J(x_1, \dots, x_n) = \int_{t_0}^{t_1} F(x_1, \dots, x_n; \dot{x}_1, \dots, \dot{x}_n, t) dt$$

Układ równań Eulera-Lagrange'a

$$F_{x_i} - \frac{d}{dt} F_{\dot{x}_i} = 0, \quad i = 1, \dots, n.$$

Warunki Legendre'a

$$F_{\dot{x}_1, \dot{x}_1} \geq 0, \quad \begin{vmatrix} F_{\dot{x}_1, \dot{x}_1} & F_{\dot{x}_1, \dot{x}_2} \\ F_{\dot{x}_2, \dot{x}_1} & F_{\dot{x}_2, \dot{x}_2} \end{vmatrix} \geq 0, \dots,$$

$$\begin{vmatrix} F_{\dot{x}_1, \dot{x}_1} & \dots & F_{\dot{x}_1, \dot{x}_n} \\ \dots & \dots & \dots \\ F_{\dot{x}_n, \dot{x}_1} & \dots & F_{\dot{x}_n, \dot{x}_n} \end{vmatrix} \geq 0.$$

Przykład dla funkcji 2-ch argumentów  $F_{\dot{x}_1, \dot{x}_1} \geq 0, \quad F_{\dot{x}_1, \dot{x}_1} F_{\dot{x}_2, \dot{x}_2} - F_{\dot{x}_1, \dot{x}_2} F_{\dot{x}_2, \dot{x}_1} \geq 0$

# Równania wyższych rzędów. Równania Eulera - Poissona

$$J(x(t)) = \int_{t_0}^{t_1} F[x(t), \dot{x}(t), \dots, x^{(n)}(t), t] dt.$$

$$F_x - \frac{d}{dt} F_{\dot{x}} + \frac{d^2}{dt^2} F_{\ddot{x}} + \dots + (-1)^n \frac{d^n}{dt^n} F_{x^{(n)}} = 0,$$

Warunek Legendre'a

$$F_{x^{(n)}, x^{(n)}} \geq 0;$$

# Zadanie

$$J(x(t)) = \int_{t_0}^{t_1} (\dot{x}^2(t) + \ddot{x}^2(t)) dt.$$

$$x(t_0) = x_0 \quad x(t_1) = x_1$$

$$\dot{x}(t_0) = \dot{x}_0 \quad \dot{x}(t_1) = \dot{x}_1$$

$$F(x, \dot{x}, \ddot{x}) = \dot{x}^2(t) + \ddot{x}^2(t)$$

$$F_x = 0$$

$$F_{\dot{x}} = 2\dot{x},$$

$$F_{\ddot{x}} = 2\ddot{x},$$

$$F_x - \frac{d}{dt} F_{\dot{x}} + \frac{d^2}{dt^2} F_{\ddot{x}} = 0,$$



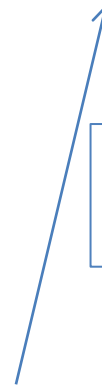
$$x^{(4)}(t) - \ddot{x}(t) = 0$$

Warunek Legendre'a

$$F_{\ddot{x}, \ddot{x}} \geq 0;$$



$$F_{\ddot{x}, \ddot{x}} = 2$$



# Rozwiązanie

$$x(t_0) = x_0$$

$$\dot{x}(t_0) = \dot{x}_0$$

$$x(t_1) = x_1$$

$$\dot{x}(t_1) = \dot{x}_1$$



$$x^{(4)}(t) - x''(t) = 0$$

Autonomous equation:

True

ODE classification:

higher-order linear ordinary differential equation



Alternate form:

$$x''(t) = x^{(4)}(t)$$

Differential equation solution:

$$x(t) = c_1 e^t + c_2 e^{-t} + c_4 t + c_3$$

derivative of  $x(t) = c_1 e^t + c_2 e^{-t} + c_4 t + c_3$

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Derivative:

$$\frac{\partial}{\partial t}(x(t) = c_1 e^t + c_2 e^{-t} + c_4 t + c_3) = c_1 e^t - c_2 e^{-t} + c_4$$

Alternate forms:

$$c_1 e^t + c_4 = c_2 e^{-t} + x'(t)$$

$$x'(t) = e^{-t} (c_1 e^{2t} - c_2 + c_4 e^t)$$

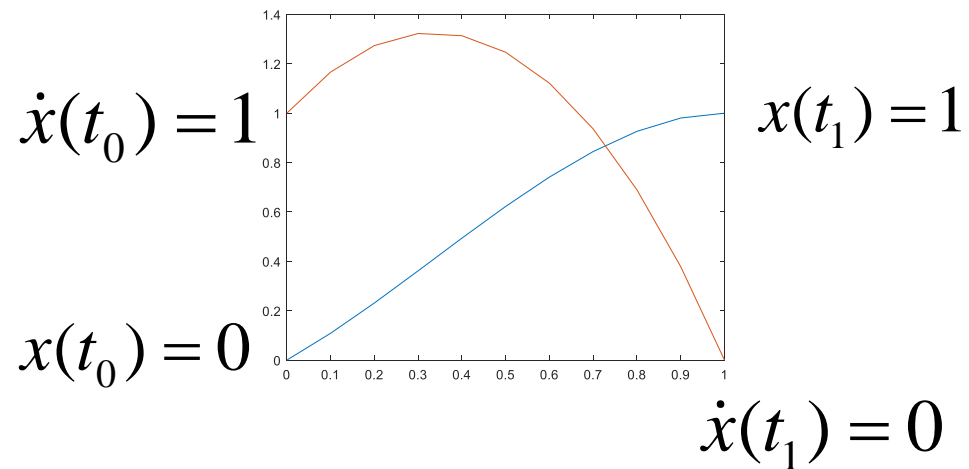
# Przykład

```
%exEP.m
clear all;
close all;
A=[1 1 0 1;
  1 -1 1 0;
  exp(1) exp(-1) 1 1;
  exp(1) -exp(-1) 1 0];
b=[0 1 1 0]';
C=A^-1*b;
Out=[];
for t=0:0.1:1
  x=C(1)*exp(t)+C(2)*exp(-t)+C(3)*t+C(4);
  dx=C(1)*exp(t)-C(2)*exp(-t)+C(3);
  Out=[Out;x dx];
end;
plot(Out(:,1));
hold on;
plot(Out(:,2));
syms t
x=C(1)*exp(t)+C(2)*exp(-t)+C(3)*t+C(4);
dxdt=diff(x,t);
d2xdt2=diff(dxdt,t);

J=vpa(int(dxdt^2+d2xdt2^2,0,1))
```

$$J = \int_{t_0}^{t_1} (\dot{x}^2(t) + \ddot{x}^2(t)) dt.$$

$$t_0 = 0 \quad t_1 = 1$$

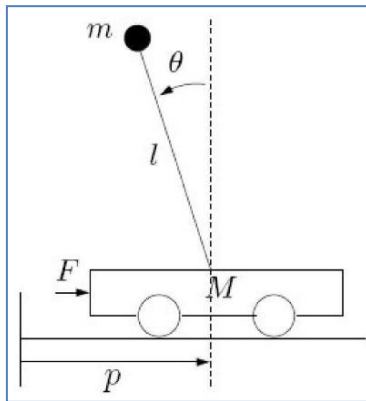


J = 5.1316234851731756135551301066122

# Sterowanie odwróconym wahadłem

MatLab - slcp

Układ składa się z wózka i zamocowanego na elastycznym przegubie pionowego wahadła o masie  $m$  i długości  $l$



Zachowanie systemu opisuje równanie różniczkowe

$$-ml^2 \frac{d^2\theta}{dt^2} + mlg \cdot \sin \theta = \tau = u(t)$$

gdzie  $\tau = u(t)$  jest sterowaniem (moment obrotowy), które należy przyłożyć w kierunku przeciwnym do wychylenia  $\theta$  aby utrzymać wahadło w pozycji pionowej.

# Sterowanie odwróconym wahadłem (cd)

$$\ddot{\varphi} + a\varphi = u \quad \int_0^T (\ddot{\varphi} - a\varphi)^2 dt$$

$$\ddot{x} - ax = u$$

$$x(0) = A; \quad x(T) = 0 \quad \dot{x}(0) = B$$

$$\dot{x}(T) = 0$$

$$F_x - \frac{d}{dt} F_{\dot{x}} + \frac{d^2}{dt^2} F_{\ddot{x}}$$

$$F = \ddot{x}^2 + 2 \ddot{x} a x + a^2 x^2$$

$$F_x = 2 \ddot{x} a + 2 a^2 x$$

$$F_{\dot{x}} = 0$$

$$F_{\ddot{x}} = 2 \ddot{x} + 2 a x$$

$$2 \ddot{x} a + 2 a^2 x + 2 \ddot{x}^2 + 2 a x^2 = 0$$

$$4 a \ddot{x} + 2 a^2 x + 2 \ddot{x}^2 = 0$$

Input

$$x^{(4)}(t) + 2a x''(t) + a^2 x(t) = 0$$

Autonomous equation

$$2a x^{(4)}(t) = -a^2 x(t) - x^{(4)}(t)$$

ODE classification

higher-order linear ordinary differential equation

Alternate form

$$x^{(4)}(t) = a^2 (-x(t)) - 2a x''(t)$$

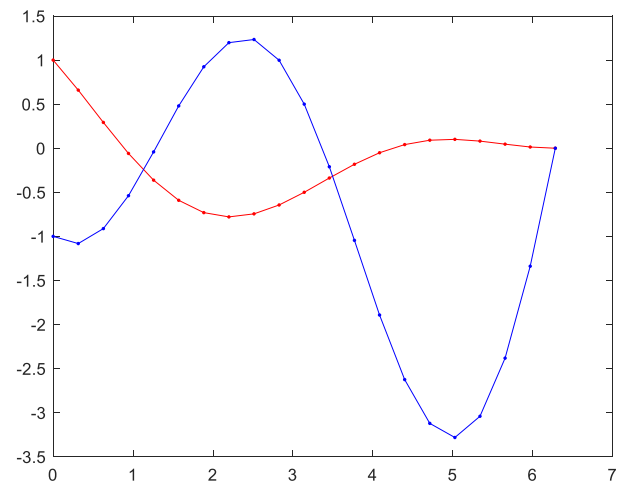
Differential equation solution

$$x(t) = c_3 \sin(\sqrt{a} t) + c_4 t \sin(\sqrt{a} t) + c_1 \cos(\sqrt{a} t) + c_2 t \cos(\sqrt{a} t)$$

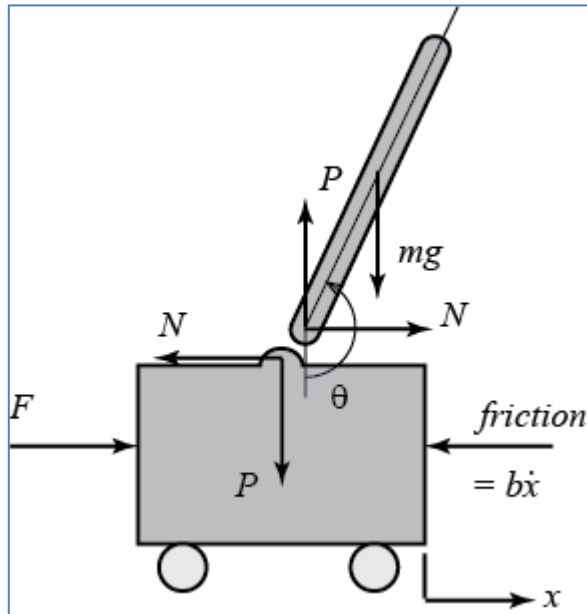


# Sterowanie odwróconym wahadłem (cd)

```
close all;
clear all;
A=1;
B=-1;
T=2*pi;
C1=A;
C2=-C1/T;
C3=B-C2;
C4=-C2-C3/T;
Out=[];
for t=0:pi/10:2*pi
x=C3*sin(t)+C4*t*sin(t)+C1*cos(t)+C2*t*cos(t)
;
dx=cos(t)*(C2+C3+C4*t)-sin(t)*(C1+C3*t-C4);
Out=[Out;t x dx];
end;
plot(Out(:,1),Out(:,2),'r.-');
hold on;
plot(Out(:,1),Out(:,3),'b.-');
```



# Wahadło odwrócone II



(M)	mass of the cart	0.5 kg
(m)	mass of the pendulum	0.2 kg
(b)	coefficient of friction for cart	0.1 N/m/sec
(l)	length to pendulum center of mass	0.3 m
(I)	mass moment of inertia of the pendulum	0.006 kg.m <sup>2</sup>
(F)	force applied to the cart	
(x)	cart position coordinate	
(theta)	pendulum angle from vertical (down)	

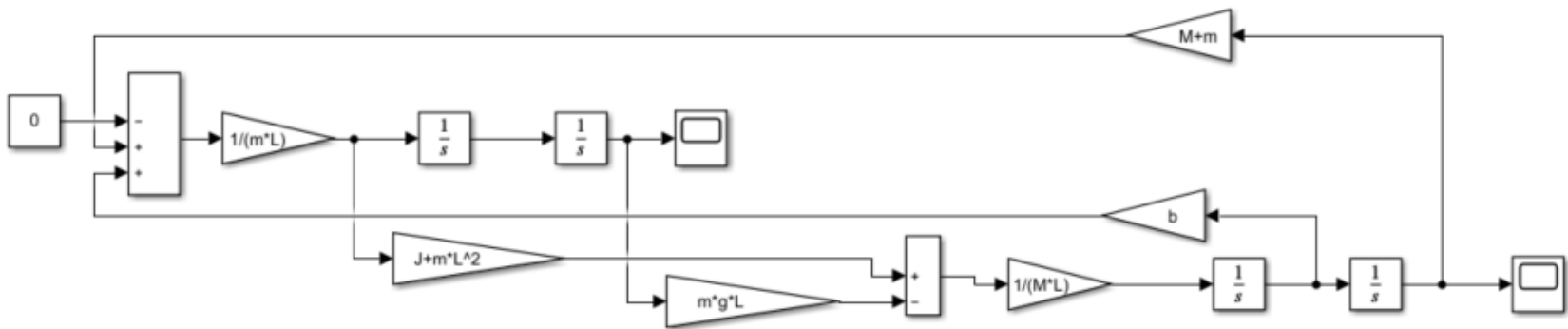
$$\begin{bmatrix} \dot{x} \\ \ddot{x} \\ \dot{\phi} \\ \ddot{\phi} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & \frac{-(I+ml^2)b}{I(M+m)+Mml^2} & \frac{m^2gl^2}{I(M+m)+Mml^2} & 0 \\ 0 & 0 & 0 & 1 \\ 0 & \frac{-mlb}{I(M+m)+Mml^2} & \frac{mgl(M+m)}{I(M+m)+Mml^2} & 0 \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \\ \phi \\ \dot{\phi} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{I+ml^2}{I(M+m)+Mml^2} \\ 0 \\ \frac{ml}{I(M+m)+Mml^2} \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \\ \phi \\ \dot{\phi} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \end{bmatrix} u$$

# Model

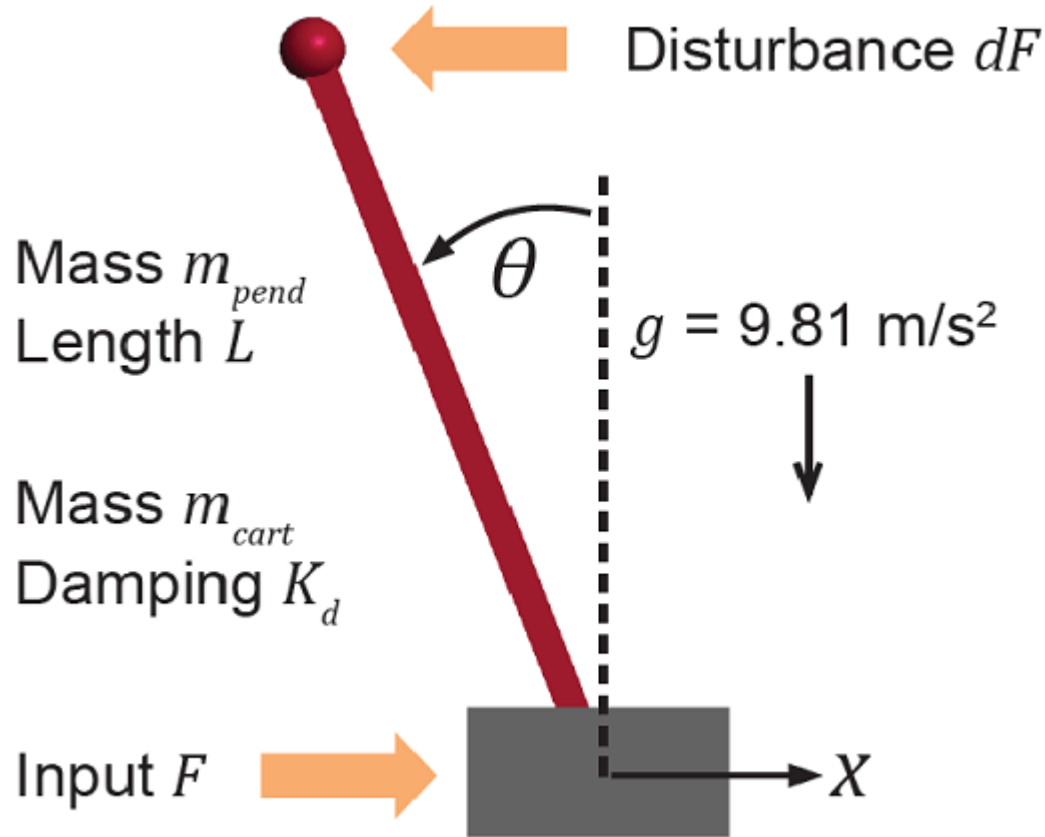
$$(J + mL^2)\ddot{\theta} - mgL\theta = mL\ddot{x}$$

$$(M + m)x + b\dot{x} - mL\ddot{\theta} = F$$

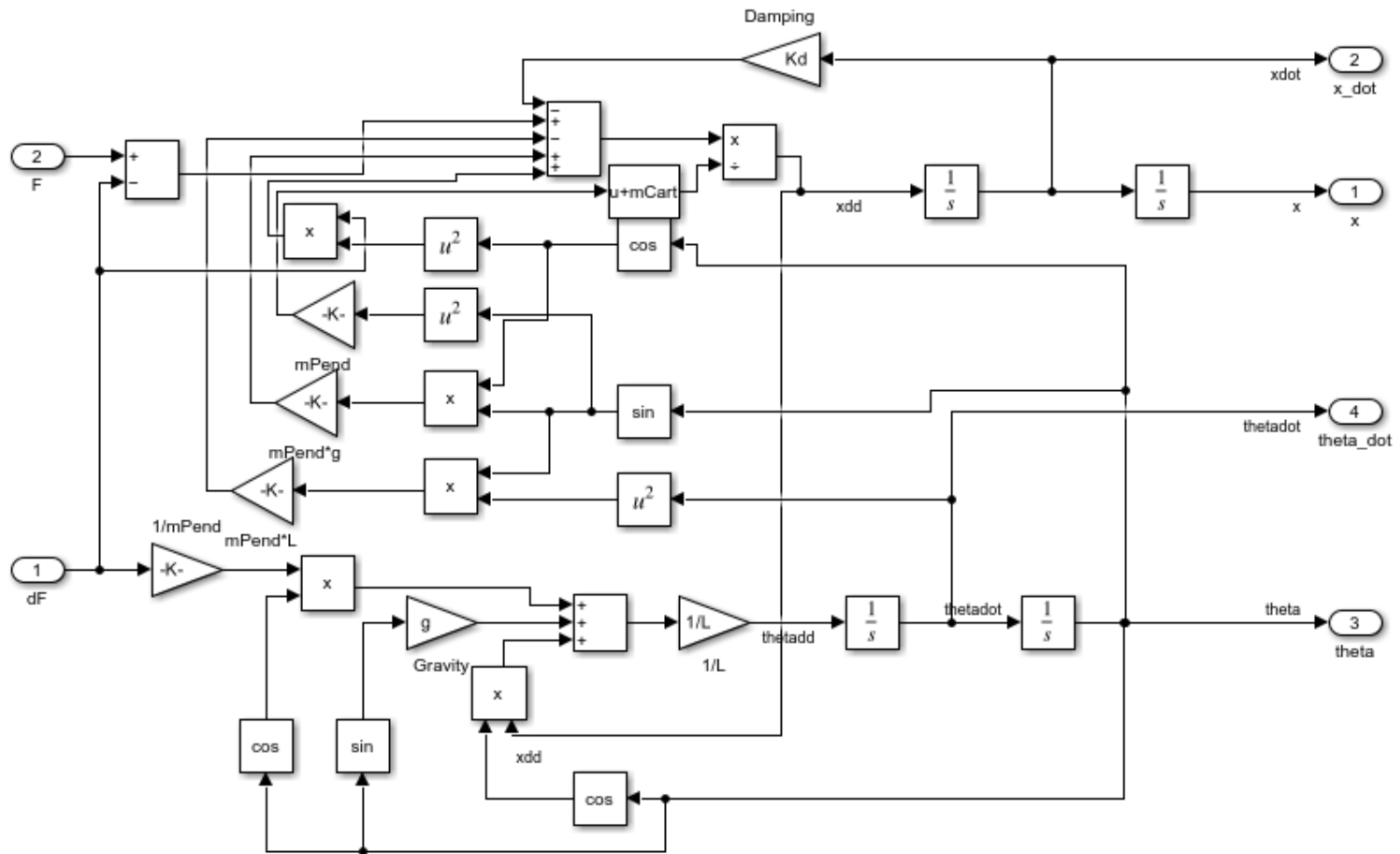


InvPendulumOS.slx

# Przykład w Matlabie

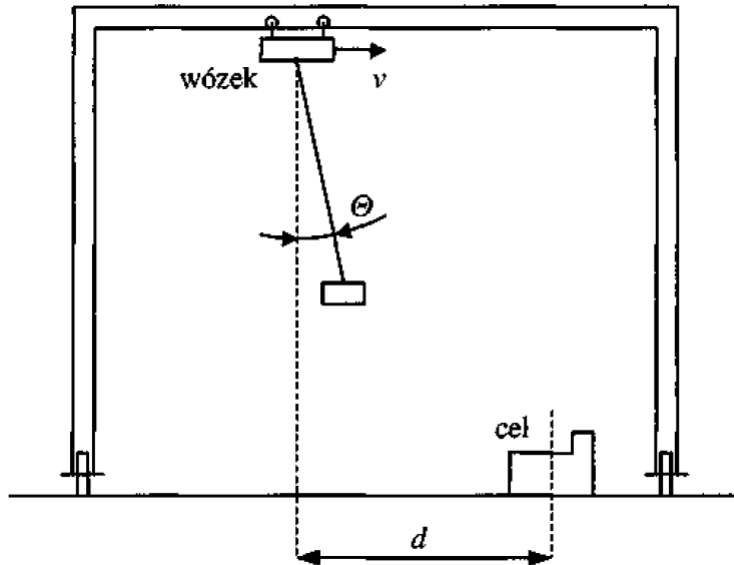


# Przykład w Matlabie (cd)



# Sterowanie wózkiem

Sterowanie wózkiem suwnicy przenoszącej kontenery z jednego miejsca w inne



Podczas transportu kontenerów dochodzi często do dużego ich kołysania (duże odchylenie  $\theta$  od pionu). Przy ustawianiu kontenera w punkcie docelowym, np. na statku, kołysania są niedopuszczalne. Na skutek uderzenia kołyszącego się kontenera w inne, już ustawione, może nastąpić ich uszkodzenie.

Operator suwnicy steruje prędkością  $v$  jej wózka przy pomocy dźwigni mającej dwa krańcowe położenia. Potrzebne jest tu **wycucie reakcji wózka**, jego bezwładności i transportowanego kontenera (**zmienny ciężar**) na zmiany położenia dźwigni. Sterowanie wózkiem suwnicy mogłoby się odbywać dwoma bardzo prostymi metodami **nie wymagającymi żadnej wiedzy eksperckiej**.

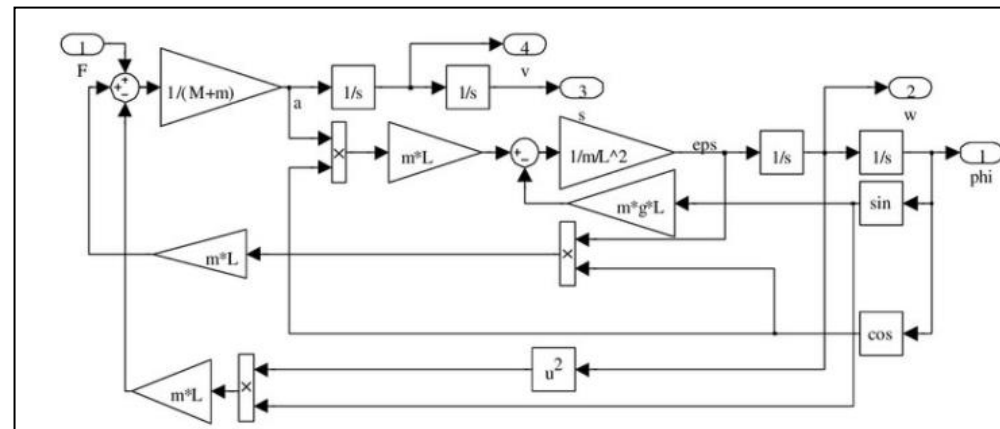
# Model wózka

$$(M + m) \frac{d^2 s(t)}{dt^2} - mL \frac{d^2 \varphi(t)}{dt^2} \cos \varphi + mL \frac{d\varphi^2(t)}{dt} \sin \varphi(t) = F(t),$$

$$- mL \frac{d^2 s(t)}{dt^2} \cos \varphi(t) + mL^2 \frac{d^2 \varphi(t)}{dt^2} + mgL \sin \varphi(t) = 0,$$

s – odległość wózka od celu

M- masa wózka, m – masa ciężaru



Linearyzacja modelu

$$\frac{d^2 s(t)}{dt^2} = a(t), \quad \frac{ds(t)}{dt} = v(t), \quad \frac{d^2 \varphi(t)}{dt^2} = \varepsilon(t), \quad \frac{d\varphi(t)}{dt} = \omega(t)$$

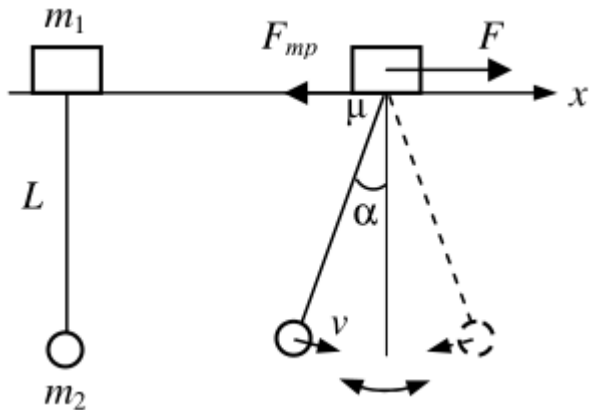
$$\varphi \approx 0, \quad \cos \varphi \approx 1, \quad \sin \varphi \approx \varphi, \quad \omega^2 \approx 0$$

$$(M + m)a(t) - mL\varepsilon(t) = F(t),$$

$$- mL a(t) + mL^2 \varepsilon(t) + mLg \varphi(t) = 0.$$

# Zagadnienie sterowania optymalnego

systema-optimalnogo-upravleniya-podveshennym-gruzom.pdf



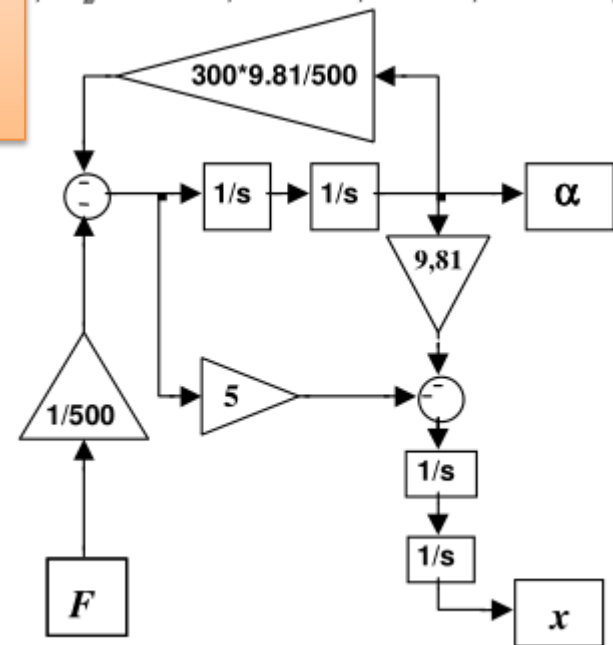
M1=100kg;  
M2=200kg;  
L=5m;  
T=5s;  
S=10m;  
Mi=0.01;

$$\begin{aligned} \alpha(0) = 0; \quad \dot{\alpha}(0) = 0; \quad x(0) = 0; \quad \dot{x}(0) = 0; \\ \alpha(T) = 0; \quad \dot{\alpha}(T) = 0; \quad \ddot{\alpha}(T) = 0; \quad x(T) = S; \\ \dot{x}(T) = 0; \quad \ddot{x}(T) = 0. \end{aligned}$$

$$\begin{cases} (m_1 + m_2)\ddot{x} + m_2L\ddot{\alpha} = F - \mu m_2 g; \\ \ddot{x} + L\ddot{\alpha} + g\alpha = 0, \end{cases}$$

$$\ddot{x} = -L\ddot{\alpha} - g\alpha$$

$$-m_1L\ddot{\alpha} - (m_1 + m_2)g\alpha = F - \mu m_2 g$$





# Optymalna trajektoria

$$\begin{aligned} \alpha(0) = 0; \quad \dot{\alpha}(0) = 0; \quad \dot{x}(0) = 0; \\ \alpha(T) = 0; \quad \dot{\alpha}(T) = 0; \quad \ddot{\alpha}(T) = 0; \\ \int_0^T \dot{x}(t) dt = S; \quad \dot{x}(T) = 0. \end{aligned}$$

$$\begin{aligned} \alpha(t) = e^{\sigma_1 t} (c_1 \cos(\beta_1 t) + c_2 \sin(\beta_1 t)) + \\ + e^{-\sigma_1 t} (c_3 \cos(\beta_1 t) + c_4 \sin(\beta_1 t)) + \\ + e^{\sigma_2 t} (c_5 \cos(\beta_2 t) + c_6 \sin(\beta_2 t)) + \\ + e^{-\sigma_2 t} (c_7 \cos(\beta_2 t) + c_8 \sin(\beta_2 t)). \end{aligned}$$

$$Q = \int_0^T (\alpha^{(4)^2} + \alpha^{(3)^2} + \ddot{\alpha}^2 + \dot{\alpha}^2 + \alpha^2) dt \rightarrow \min$$

$$\frac{\partial \Phi}{\partial \alpha} - \frac{d}{dt} \frac{\partial \Phi}{\partial \dot{\alpha}} + \frac{d^2}{dt^2} \frac{\partial \Phi}{\partial \ddot{\alpha}} - \frac{d^3}{dt^3} \frac{\partial \Phi}{\partial \alpha^{(3)}} + \frac{d^4}{dt^4} \frac{\partial \Phi}{\partial \alpha^{(4)}} = 0.$$

$$2\alpha - 2\ddot{\alpha} + 2\alpha^{(4)} - 2\alpha^{(6)} + 2\alpha^{(8)} = 0.$$

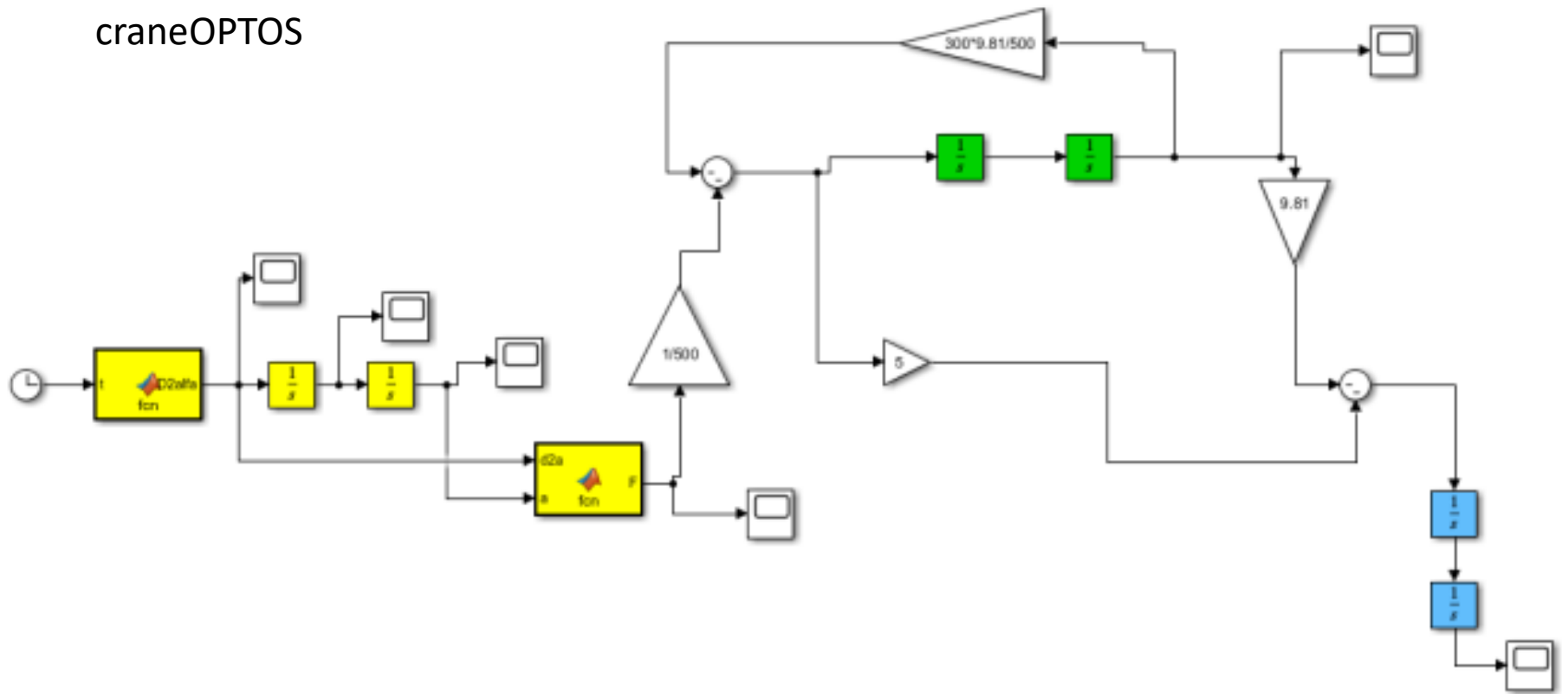
$$p^8 - p^6 + p^4 - p^2 + 1 = 0,$$

$$p_{1,2} = \sigma_1 \pm \beta_1 i; \quad p_{3,4} = -\sigma_1 \pm \beta_1 i; \quad p_{5,6} = \sigma_2 \pm \beta_2 i; \\ p_{7,8} = -\sigma_2 \pm \beta_2 i,$$

$$\sigma_1 = 0,25\sqrt{10 - 2\sqrt{5}}; \quad \sigma_2 = 0,25\sqrt{10 + 2\sqrt{5}};$$

$$\beta_1 = 0,25(1 + \sqrt{5}); \quad \beta_2 = 0,25(-1 + \sqrt{5}).$$

craneOPTOS



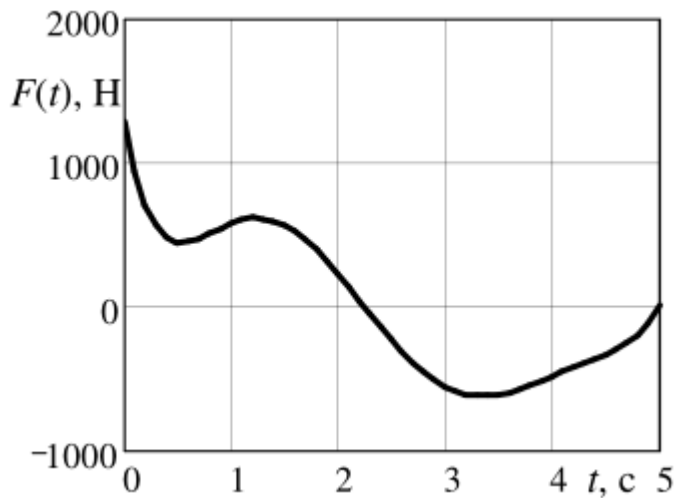
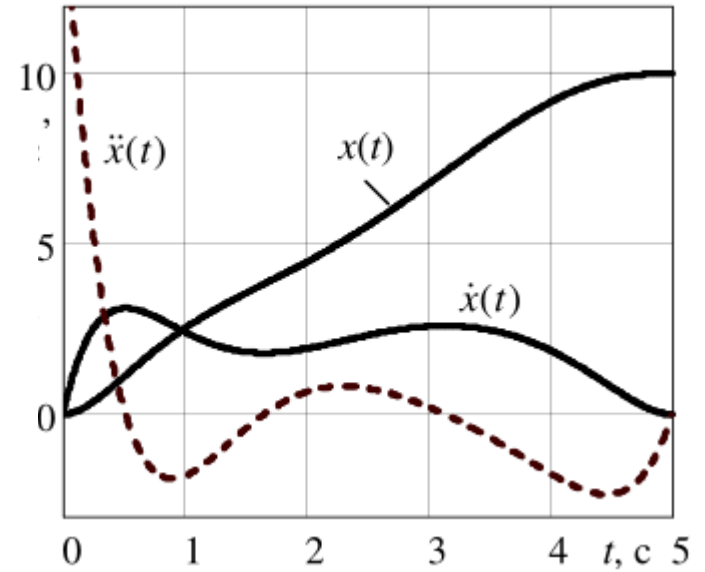
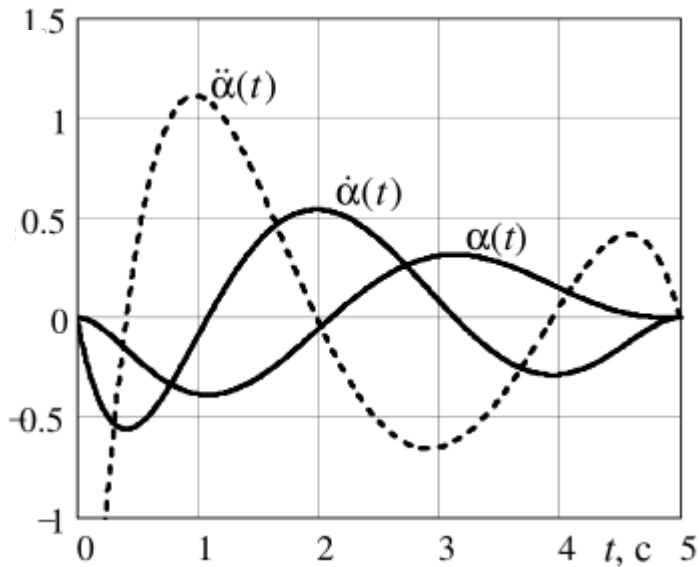
и, далее, искомые коэффициенты:  $c_1=0,202$ ;  $c_2=-0,000723$ ;  $c_3=-1,24$ ;  $c_4=-7,42$ ;  $c_5=0,0724$ ;  $c_6=0,014$ ;  $c_7=0,961$ ;  $c_8=19,4$ .

craneOPTOS

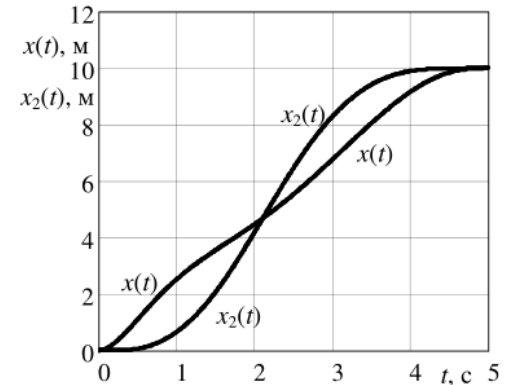
```
function D2alfa = fcn(t)
c1=0.202;c2=-0.000723;c3=-1.24;c4=-7.42;c5=0.0724;
c6=0.014;c7=0.961;c8=19.4;
s1=0.25*sqrt(10-2*sqrt(5));
s2=0.25*sqrt(10+2*sqrt(5));
b1=0.25*(1+sqrt(5));
b2=0.25*(-1+sqrt(5));
%syms s1 s2 b1 b2 c1 c2 c3 c4 c5 c6 c7 c8 t
%alfa =exp(s1*t)*(c1*cos(b1*t)+c2*sin(b1*t))+exp(-
s1*t)*(c3*cos(b1*t)+c4*sin(b1*t))+exp(s2*t)*(c5*cos(b2*t)+c6*sin(b2*t))+exp(-
s2*t)*(c7*cos(b2*t)+c8*sin(b2*t));
```

```
function F = fcn(d2a,a)
m1=100;m2=200;L=5;g=9.81;mi=0.01;
F=mi*m2*g-m1*L*d2a-
(m1+m2)*g*a;
```

```
%Dalfa=diff(alfa);
%D2alfa=diff(Dalfa);
D2alfa=s1^2*exp(s1*t)*(c1*cos(b1*t) + c2*sin(b1*t)) - exp(-s1*t)*(b1^2*c3*cos(b1*t)
+ b1^2*c4*sin(b1*t)) - exp(s2*t)*(b2^2*c5*cos(b2*t) + b2^2*c6*sin(b2*t)) - exp(-
s2*t)*(b2^2*c7*cos(b2*t) + b2^2*c8*sin(b2*t)) - exp(s1*t)*(b1^2*c1*cos(b1*t) +
b1^2*c2*sin(b1*t)) + s1^2*exp(-s1*t)*(c3*cos(b1*t) + c4*sin(b1*t)) +
s2^2*exp(s2*t)*(c5*cos(b2*t) + c6*sin(b2*t)) + s2^2*exp(-s2*t)*(c7*cos(b2*t) +
c8*sin(b2*t)) + 2*s1*exp(s1*t)*(b1*c2*cos(b1*t) - b1*c1*sin(b1*t)) - 2*s1*exp(-
s1*t)*(b1*c4*cos(b1*t) - b1*c3*sin(b1*t)) + 2*s2*exp(s2*t)*(b2*c6*cos(b2*t) -
b2*c5*sin(b2*t)) - 2*s2*exp(-s2*t)*(b2*c8*cos(b2*t) - b2*c7*sin(b2*t))
```

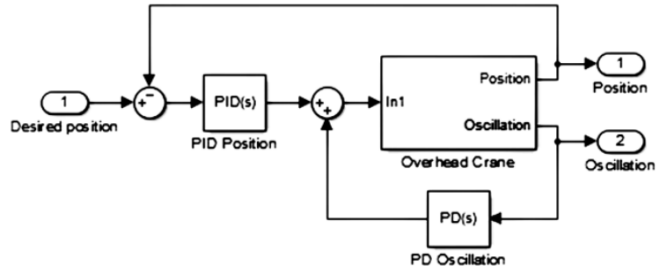


$$x_2(t) = x(t) + L \sin \alpha(t)$$

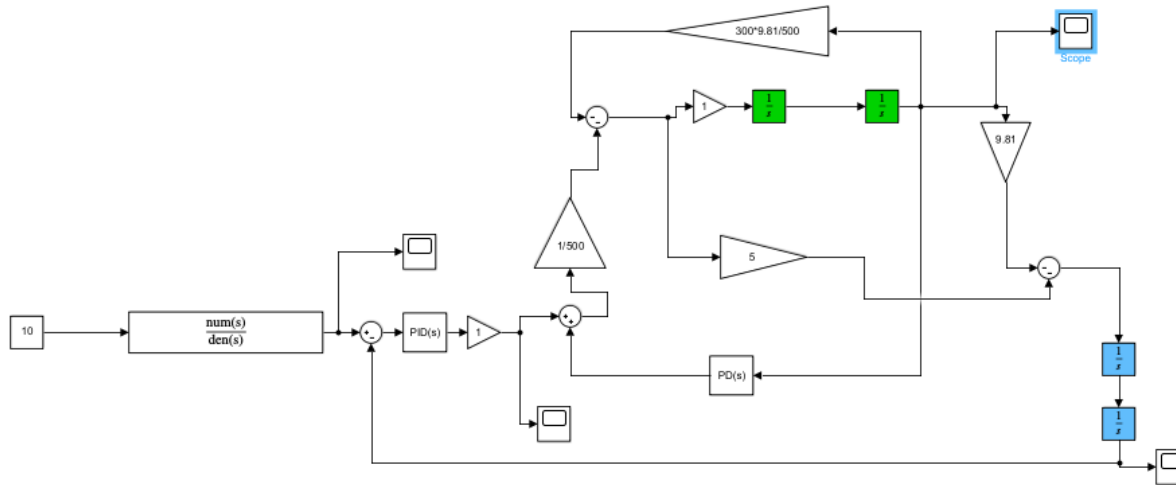


Ruch wózka i ładunku jest jednostajny: na początku ruchu ( $t < 2,1$  s) ładunek pozostaje w tyle za wózkiem, a następnie, zbliżając się do współrzędnej  $x = 10$  m, wyprzedza go i w punkcie  $x = 10$ ,  $x_2 = 10$  układ bez wahanja kończy ruch.

# PID



cranePIDPDOS



Block Parameters: PID Controller

PID 1dof (mask) (link)

This block implements continuous- and discrete-time PID control algorithms and includes advanced features such as anti-windup, external reset, and signal tracking. You can tune the PID gains automatically using the 'Tune...' button (requires Simulink Control Design).

Controller: PID

Form: Parallel

Time domain:

- Continuous-time
- Discrete-time

Discrete-time settings

Sample time (-1 for inherited): -1

Compensator formula

$$P + I \frac{1}{s} + D \frac{N}{1 + N \frac{1}{s}}$$

Main Initialization Output Saturation Data Types State Attributes

Controller parameters

Source: internal

Proportional (P): 2751.62854455126

Integral (I): 94.1124942564012

Derivative (D): 19759.9982056351

Use filtered derivative

Filter coefficient (N): 3.88278564322259

Automated tuning

OK Cancel Help Apply

Block Parameters: PID Controller1

PID 1dof (mask) (link)

This block implements continuous- and discrete-time PID control algorithms and includes advanced features such as anti-windup, external reset, and signal tracking. You can tune the PID gains automatically using the 'Tune...' button (requires Simulink Control Design).

Controller: PD Form: Parallel

Time domain:

Continuous-time

Discrete-time

Discrete-time settings

Sample time (-1 for inherited): -1

▼ Compensator formula

$$P + D \frac{N}{1 + N \frac{1}{s}}$$

Main Initialization Output Saturation Data Types State Attributes

Controller parameters

Source: internal

Proportional (P): 204370.101008071

Derivative (D): 21515.6538274445

Use filtered derivative

Filter coefficient (N): 5053.95249806519

Automated tuning

Select tuning method: Transfer Function Based (PID Tuner App) Tune...

OK Cancel Help Apply

Block Parameters: Transfer Fcn

**Transfer Fcn**

The numerator coefficient can be a vector or matrix expression. The denominator coefficient must be a vector. The output width equals the number of rows in the numerator coefficient. You should specify the coefficients in descending order of powers of s.

**Parameters**

Numerator coefficients:

Denominator coefficients:

Absolute tolerance:

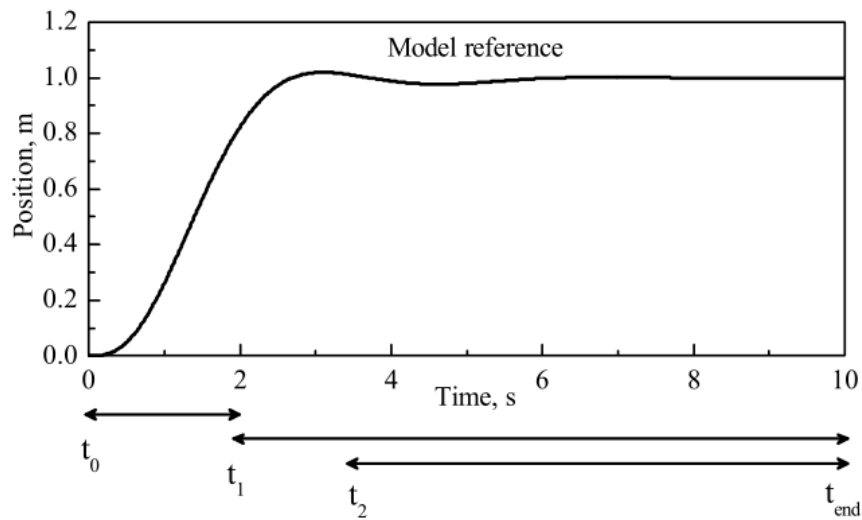
State Name: (e.g., 'position')

?

OK Cancel Help Apply



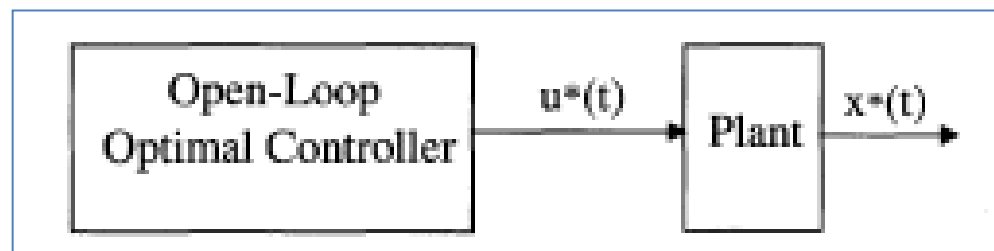


$$J = \int_0^{t_1} t(x - x_{ref})^2 dt + \int_{t_1}^{t_{end}} t(\theta)^2 dt + \int_{t_2}^{t_{end}} t(x - x_{ref})^2 dt$$

$$X_{ref} = \frac{\omega^3}{s^3 + 1.75\omega s^2 + 2.15\omega^2 s + 1.5\omega^3}$$

# Typy układów sterowania

Układ otwarty

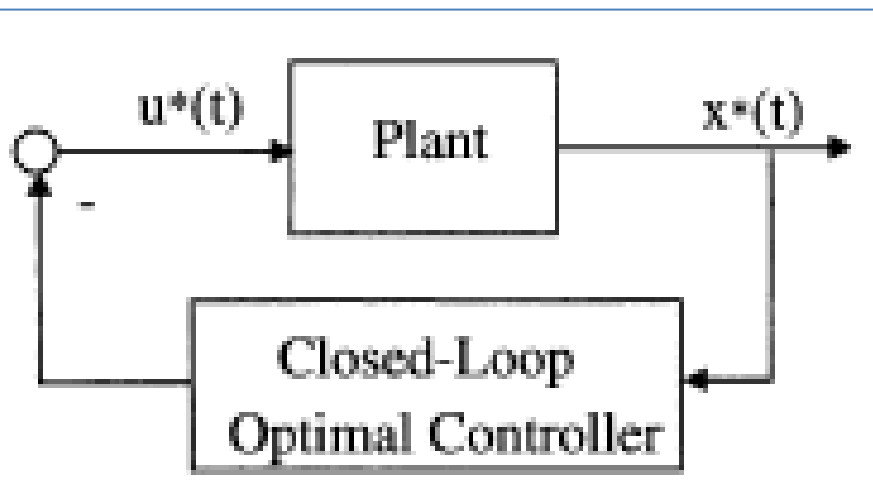


Sterowanie w układzie otwartym (ręczne lub automatyczne) polega na takim nastawieniu wielkości wejściowej, aby znając charakterystykę obiektu i przewidując możliwość działania nań zakłóceń, otrzymać na wyjściu pożądaną wartość. Ponieważ nie istnieje możliwość tłumienia nieznanych zakłóceń oraz osiągnięcie wartości zadanej nie może być zweryfikowane, układ otwarty stosowany jest w przypadku prostych obiektów, dla których znany jest dokładny model matematyczny. W przypadku znanej wartości zakłócenia (np. temperatury na zewnątrz budynku, w którym znajduje się kocioł centralnego ogrzewania) układ otwarty może być użyty do jego kompensacji.

**Podstawową wadą takiego rodzaju sterowania jest wpływ dynamiki układu na wartość wyjściową.** W porównaniu do układu regulacji układ otwarty jest bardziej czuły na zmiany wzmocnienia statycznego w układzie.

# Typy układów sterowania

Układ zamknięty - **Regulator ze sprzężeniem zwrotnym**



Układ zamknięty (ang. closed-loop system) – układ sterowania, w którym przebieg sygnału następuje w dwóch kierunkach. Od wejścia do wyjścia przebiega sygnał realizujący wzajemne oddziaływanie elementów, natomiast od wyjścia do wejścia przebiega sygnał sprzężenia zwrotnego.

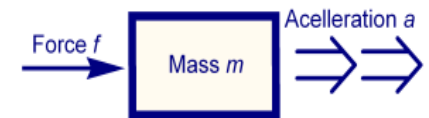
Sterowanie w układzie zamkniętym (ręczne lub automatyczne) różni się od sterowania w układzie otwartym tym, że człowiek lub regulator otrzymują dodatkowo poprzez sprzężenie zwrotne informacje o stanie wielkości wyjściowej (lub o stanie obiektu). Informacja ta (odczytana z miernika lub podana w postaci np. napięcia do regulatora) jest używana do korygowania nastaw wielkości wejściowej.

# Optymalizacja układu dynamicznego

$$\frac{d^2 x(t)}{dt^2} = u(t)$$

$$\begin{cases} \dot{x}_1(t) = x_2(t), \\ \dot{x}_2(t) = u(t), \end{cases} \quad \begin{matrix} x_1 = x, & x_2 = \dot{x}_1 = \dot{x} \\ x_1(0) = x_{10} = 1, & x_1(T) = x_{1T} = 0,25, \\ x_2(0) = x_{20} = 1, & x_2(T) = x_{2T} = 0, \\ & T = 5 \text{ s.} \end{matrix}$$

$$f = m \cdot a$$



$$\begin{aligned} x_1(0) &= x_{10}, & x_1(T) &= x_{1T}, \\ x_2(0) &= x_{20}, & x_2(T) &= x_{2T}, \\ t_0 &= 0, & t_1 &= T. \end{aligned}$$

$$J = \int_0^T u^2(t) dt \rightarrow \min$$

$$J(x(t)) = \int_0^T \ddot{x}^2(t) dt.$$

# Rozwiązanie

$$F(x) = \left( \frac{d^2 x}{dt^2} \right)^2; F_x = \frac{\partial F}{\partial x} = 0; \quad F_{\dot{x}} = \frac{\partial F}{\partial \dot{x}} = 0; \quad F_{\ddot{x}} = \frac{\partial F}{\partial \ddot{x}} = 2 \frac{d^2 x}{dt^2}.$$

$$F_x - \frac{d}{dt} F_{\dot{x}} + \frac{d^2}{dt^2} F_{\ddot{x}} = 0,$$

Rozwiązanie



$$2 \frac{d^4 x}{dt^4} = 0. \quad \longrightarrow$$

Całkując dwa razy otrzymamy

$$\begin{cases} \dot{x}_1(t) = x_2(t), \\ \dot{x}_2(t) = u(t), \end{cases}$$

$$u(t) = \ddot{x}(t) = \dot{x}_2(t) = C_1 t + C_2$$

$x'''=0$

 Extended Keyboard  Upl

Assuming ' is referring to math | U

Input:

$x^{(4)}(t) = 0$

ODE names:

Euler-Cauchy equation

$x^{(4)}(t) = 0$

Autonomous equation

$x^{(4)}(t) = 0$

Differential equation solution:

$x(t) = c_4 t^3 + c_3 t^2 + c_2 t + c_1$

# Rozwiązanie

Całkując dalej otrzymamy

$$x_2(t) = \frac{C_1}{2}t^2 + C_2t + C_3;$$

$$x_1(t) = \frac{C_1}{6}t^3 + \frac{C_2}{2}t^2 + C_3t + C_4.$$

Spełnienie warunków

$$x_1(0) = x_{10} = 1, \quad x_1(T) = x_{1T} = 0,25,$$

$$x_2(0) = x_{20} = 1, \quad x_2(T) = x_{2T} = 0,$$

$$T = 5 \text{ s.}$$

$$t = 0 \quad 1 = C_3, \quad 1 = C_4;$$

$$t = T = 5$$

$$0 = \frac{C_1}{2}25 + C_25 + 1,$$

$$0,25 = \frac{C_1}{6}125 + \frac{C_2}{2}25 + 5 + 1.$$

# Rozwiązanie systemu w MatLabie

```
>> syms c1 c2
eq1= c1*(25/2)+c2*5+1;
eq2= c1*(125/6)+c2*(25/2)+6-0.25;
[c1,c2]= solve(eq1, eq2)
```

```
c1 =
39/125
```

```
c2 =
-49/50
```

```
>> c1=39/125
```

```
c1 =
0.3120
```

```
>> c2=-49/50
```

```
c2 =
-0.9800
```

$$C_1 = 0,312$$

$$C_2 = -0,980$$

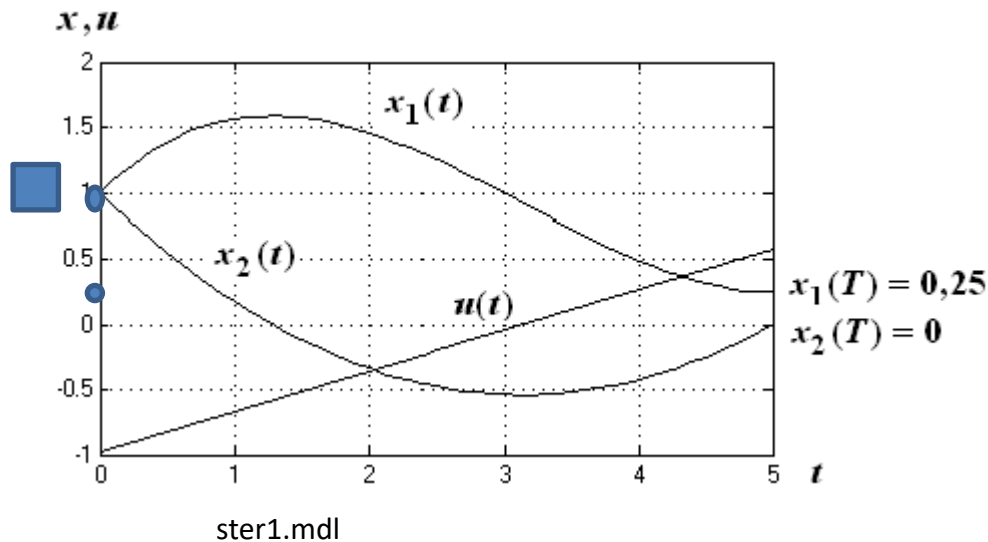
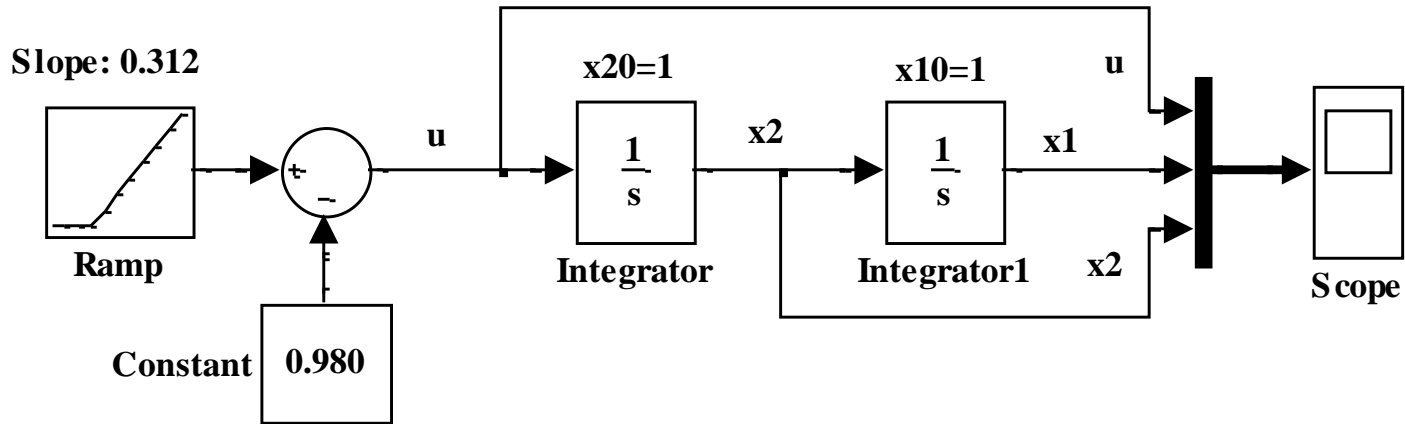
Warunek Legende'a

$$F_{\ddot{x},\ddot{x}} = \frac{\partial F_{\ddot{x}}}{\partial \ddot{x}} = 2 > 0.$$

$$\mathbf{u(t) = 0,312t - 0,980.}$$

Sterowanie programowe

# Symulacja



$$J = \int_0^T u^2(t) dt \rightarrow \min$$



# U=0

$$\frac{d^2 x(t)}{dt^2} = u(t) = 0$$

---

$$x''(t) = 0$$

ODE names:

Euler-Cauchy equation

$$x''(t) = 0$$

---

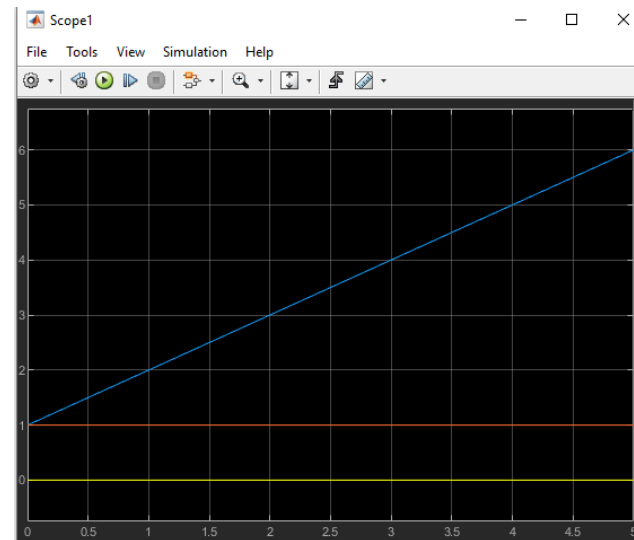
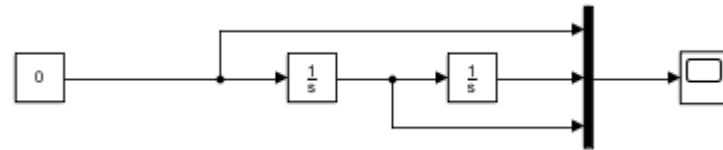
Autonomous equation

$$x''(t) = 0$$

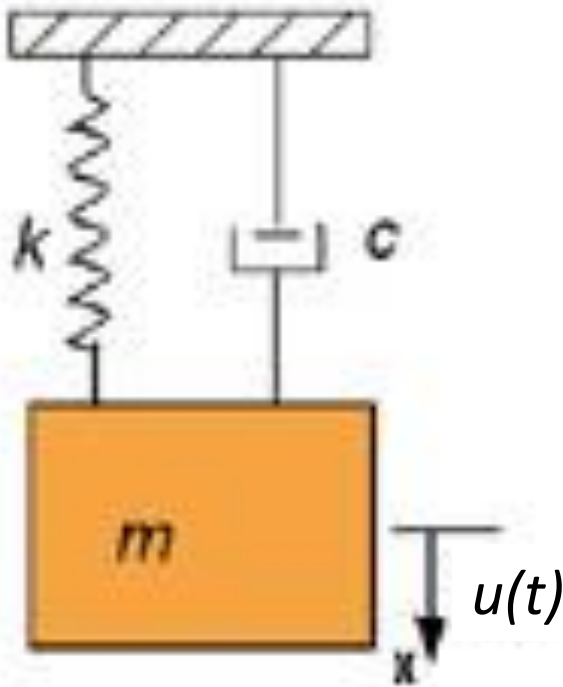
---

Differential equation solution:

$$x(t) = c_2 t + c_1$$



# Oscylator harmoniczny tłumiony



$$\frac{d^2 x(t)}{dt^2} + c \frac{dx(t)}{dt} + Kx(t) = u(t)$$

$$J = \int_{t_0}^{t_1} u^2(t) dt \rightarrow \min$$

$$x(t_0) = x_0 \quad \dot{x}(t_0) = \dot{x}_0 \quad x(t_1) = x_1 \quad \dot{x}(t_1) = \dot{x}_1$$

$$J(x(t)) = \int_{t_0}^{t_1} \left( \frac{d^2 x(t)}{dt^2} + c \frac{dx(t)}{dt} + Kx(t) \right)^2 dt$$

$$F = (\ddot{x} + c\dot{x} + Kx)^2$$

$$F = (\ddot{x} + c\dot{x} + Kx)^2$$

$$F_x - \frac{d}{dt} F_{\dot{x}} + \frac{d^2}{dt^2} F_{\ddot{x}} = 0,$$

$$F_x = 2K(\ddot{x} + c\dot{x} + Kx)$$

$$F_{\dot{x}} = 2c(\ddot{x} + c\dot{x} + Kx)$$

$$F_{\ddot{x}} = 2(\ddot{x} + c\dot{x} + Kx)$$

$$F_x = 2K(\ddot{x} + c\dot{x} + Kx) \quad \frac{d}{dt} F_{\dot{x}} = 2c(\ddot{x} + c\dot{x} + Kx)$$

$$\frac{d^2}{dt^2} F_{\ddot{x}} = 2(\ddot{\ddot{x}} + c\ddot{\dot{x}} + K\ddot{x}) \quad F_x - \frac{d}{dt} F_{\dot{x}} + \frac{d^2}{dt^2} F_{\ddot{x}} = 0,$$

$$2\ddot{\ddot{x}} + (4K - 2c^2)\ddot{\dot{x}} + 2K^2x = 0$$

$$2\ddot{x} + (4K - 2c^2)\dot{x} + 2K^2x = 0$$

$$x(t) = C_1 e^{tK_1} + C_2 e^{tK_2} + C_3 e^{-tK_1} + C_4 e^{-tK_2}$$

$$K_1 = \left( \frac{c}{2} - \frac{(c^2 - 4K)^{1/2}}{2} \right)$$

$$K_2 = \left( \frac{c}{2} + \frac{(c^2 - 4K)^{1/2}}{2} \right)$$

# Program

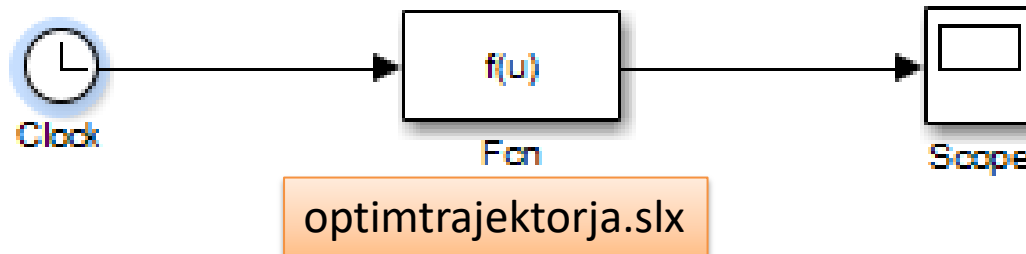
sprezynaSYM.m

```
clear all
disp('Rozwiazanie')
syms t x Dx D2x D3x D4x c K
F=(D2x+c*Dx+K*x)^2;
t1=0;
x1=0;
dx1=0;
t2=1;
x2=1;
dx2=0;
dFdx=diff(F,x);
%2*K*(D2x + Dx*c + K*x)
dFdDx=diff(F,Dx);
%2*c*(D2x + Dx*c + K*x)
dFdD2x=diff(F,D2x);
%2*D2x + 2*Dx*c + 2*K*x
dFdtDdx=2*c*(D3x+c*D2x+K*Dx);
d2Fdt2dFdD2x=2*(D4x+c*D3x+K*D2x);
%Poisson
Poisson=simple(dFdx-dFdtDdx+d2Fdt2dFdD2x);
%2*x*K^2 + 4*D2x*K - 2*D2x*c^2 + 2*D4x
deqPoisson=[char(Poisson) '=0'];
Sol=dsolve(deqPoisson,'t');
%C2*exp(t*(c/2 + (c^2 - 4*K)^(1/2)/2)) + C3*exp(t*(c/2 - (c^2 - 4*K)^(1/2)/2)) + C4*exp(-t*(c/2 - (c^2 - 4*K)^(1/2)/2)) + C5*exp(-t*(c/2 + (c^2 - 4*K)^(1/2)/2))
dSoldt= diff(Sol,t);
SolLeft=subs(Sol,t,t1); % t1
%C2 + C3 + C4 + C5
SolRight=subs(Sol,t,t2); % t2
%C2*exp(c/2 + (c^2 - 4*K)^(1/2)/2) + C3*exp(c/2 - (c^2 - 4*K)^(1/2)/2) + C4*exp((c^2 - 4*K)^(1/2)/2 - c/2) + C5*exp(- c/2 - (c^2 - 4*K)^(1/2)/2)
difSolLeft=subs(dSoldt,t,t1); % t1
%C2*(c/2 + (c^2 - 4*K)^(1/2)/2) + C3*(c/2 - (c^2 - 4*K)^(1/2)/2) - C4*(c/2 - (c^2 - 4*K)^(1/2)/2) - C5*(c/2 + (c^2 - 4*K)^(1/2)/2)
difSolRight=subs(dSoldt,t,t2); % t2
%C2*exp(c/2 + (c^2 - 4*K)^(1/2)/2)*(c/2 + (c^2 - 4*K)^(1/2)/2) + C3*exp(c/2 - (c^2 - 4*K)^(1/2)/2)*(c/2 - (c^2 - 4*K)^(1/2)/2) - C4*exp((c^2 - 4*K)^(1/2)/2 - c/2)*(c/2 - (c^2 - 4*K)^(1/2)/2) - C5*exp(-
c/2 - (c^2 - 4*K)^(1/2)/2)*(c/2 + (c^2 - 4*K)^(1/2)/2)
EqLeft=[char(SolLeft) '=' char(sym(x1))]; % =x1
EqRight=[char(SolRight) '=' char(sym(x2))]; % =x2
EqLeft2=[char(difSolLeft) '=' char(sym(dx1))]; % =x1
EqRight2=[char(difSolRight) '=' char(sym(dx2))]; % =x2
Con=solve(EqLeft,EqRight,EqLeft2,EqRight2,'C2,C3,C4,C5');
C2=Con.C2;
C3=Con.C3;
C4=Con.C4;
C5=Con.C5;

Sol21=vpa(eval(Sol),14);
dSol21=diff(Sol21,t);
d2Sol21=diff(dSol21,t);
```

# Rozwiązanie

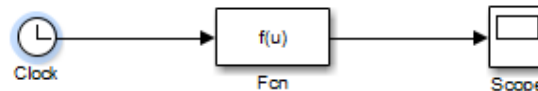
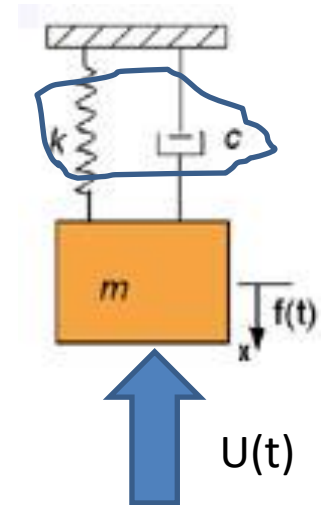
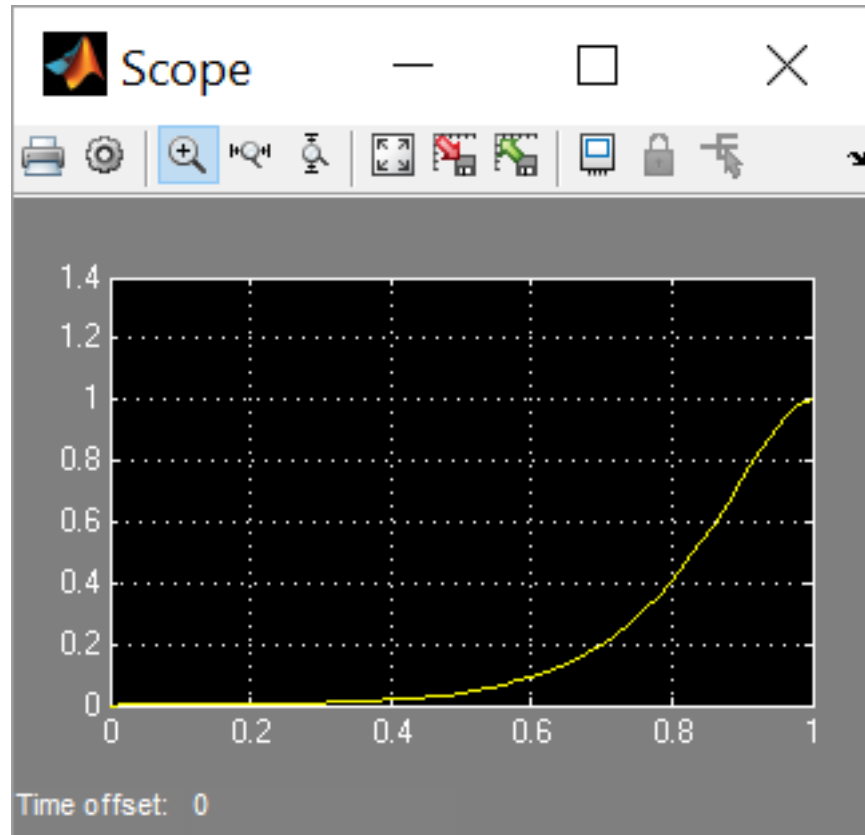
$$\begin{aligned} & (0.5 * \exp(u(1) * (0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2}))) * (1.0 * \exp(0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2})) * (4.0 * K - 1.0 * c^2) - c^2 * \exp(-0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) - \\ & \exp(-0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) * (4.0 * K - 1.0 * c^2) + 1.0 * c^2 * \exp(0.5 * (c^2 - 4.0 * K)^{1/2} - 0.5 * c) + 1.0 * c * \exp(0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) * (c^2 - \\ & 4.0 * K)^{1/2} - c * \exp(0.5 * (c^2 - 4.0 * K)^{1/2} - 0.5 * c) * (c^2 - 4.0 * K)^{1/2} / (c^2 * \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2})) * \exp(0.5 * (c^2 - 4.0 * K)^{1/2} - 0.5 * c) - \\ & 8.0 * K + c^2 * \exp(-0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) * \exp(0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) + \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2}) * \exp(0.5 * c - 0.5 * (c^2 - \\ & 4.0 * K)^{1/2}) * (4.0 * K - 1.0 * c^2) + \exp(-0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) * \exp(0.5 * (c^2 - 4.0 * K)^{1/2} - 0.5 * c) * (4.0 * K - 1.0 * c^2) - (0.5 * \exp(-1.0 * u(1) * (0.5 * c - \\ & 0.5 * (c^2 - 4.0 * K)^{1/2}))) * (\exp(0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2})) * (4.0 * K - 1.0 * c^2) - 1.0 * c^2 * \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2}) - 1.0 * \exp(-0.5 * c - 0.5 * (c^2 - \\ & 4.0 * K)^{1/2}) * (4.0 * K - 1.0 * c^2) + c^2 * \exp(0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) - 1.0 * c * \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2}) * (c^2 - 4.0 * K)^{1/2} + c * \exp(-0.5 * c - \\ & 0.5 * (c^2 - 4.0 * K)^{1/2}) * (c^2 - 4.0 * K)^{1/2} / (c^2 * \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2})) * \exp(0.5 * (c^2 - 4.0 * K)^{1/2} - 0.5 * c) - 8.0 * K + c^2 * \exp(-0.5 * c - \\ & 0.5 * (c^2 - 4.0 * K)^{1/2}) * \exp(0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) + \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2}) * \exp(0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) * (4.0 * K - 1.0 * c^2) + \\ & \exp(-0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) * \exp(0.5 * (c^2 - 4.0 * K)^{1/2} - 0.5 * c) * (4.0 * K - 1.0 * c^2) + (0.5 * \exp(-1.0 * u(1) * (0.5 * c + 0.5 * (c^2 - \\ & 4.0 * K)^{1/2}))) * (\exp(0.5 * (c^2 - 4.0 * K)^{1/2} - 0.5 * c) * (4.0 * K - 1.0 * c^2) - 1.0 * c^2 * \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2}) - 1.0 * \exp(0.5 * c + 0.5 * (c^2 - \\ & 4.0 * K)^{1/2}) * (4.0 * K - 1.0 * c^2) + c^2 * \exp(0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) - 1.0 * c * \exp(0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) * (c^2 - 4.0 * K)^{1/2} + c * \exp(0.5 * (c^2 \\ & 4.0 * K)^{1/2} - 0.5 * c) * (c^2 - 4.0 * K)^{1/2} / (c^2 * \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2})) * \exp(0.5 * (c^2 - 4.0 * K)^{1/2} - 0.5 * c) - 8.0 * K + c^2 * \exp(-0.5 * c - 0.5 * (c^2 - \\ & 4.0 * K)^{1/2}) * \exp(0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) + \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2}) * \exp(0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) * (4.0 * K - 1.0 * c^2) + \exp(- \\ & 0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) * \exp(0.5 * (c^2 - 4.0 * K)^{1/2} - 0.5 * c) * (4.0 * K - 1.0 * c^2) - (0.5 * \exp(u(1) * (0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}))) * (1.0 * \exp(0.5 * (c^2 - \\ & 4.0 * K)^{1/2} - 0.5 * c) * (4.0 * K - 1.0 * c^2) - c^2 * \exp(-0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) - \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2}) * (4.0 * K - 1.0 * c^2) + \\ & 1.0 * c^2 * \exp(0.5 * (c^2 - 4.0 * K)^{1/2} - 0.5 * c) + 1.0 * c * \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2}) * (c^2 - 4.0 * K)^{1/2} - c * \exp(-0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) * (c^2 \\ & 4.0 * K)^{1/2} / (c^2 * \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2})) * \exp(0.5 * (c^2 - 4.0 * K)^{1/2} - 0.5 * c) - 8.0 * K + c^2 * \exp(-0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) * \exp(0.5 * c \\ & 0.5 * (c^2 - 4.0 * K)^{1/2}) + \exp(0.5 * c + 0.5 * (c^2 - 4.0 * K)^{1/2}) * \exp(0.5 * c - 0.5 * (c^2 - 4.0 * K)^{1/2}) * (4.0 * K - 1.0 * c^2) + \exp(-0.5 * c - 0.5 * (c^2 - \\ & 4.0 * K)^{1/2}) * \exp(0.5 * (c^2 - 4.0 * K)^{1/2} - 0.5 * c) * (4.0 * K - 1.0 * c^2) \end{aligned}$$





# Symulacja. Trajektoria optymalna.

**t1=0;**  
**x1=0;**  
**dx1=0;**  
**t2=1;**  
**x2=1;**  
**dx2=0;**

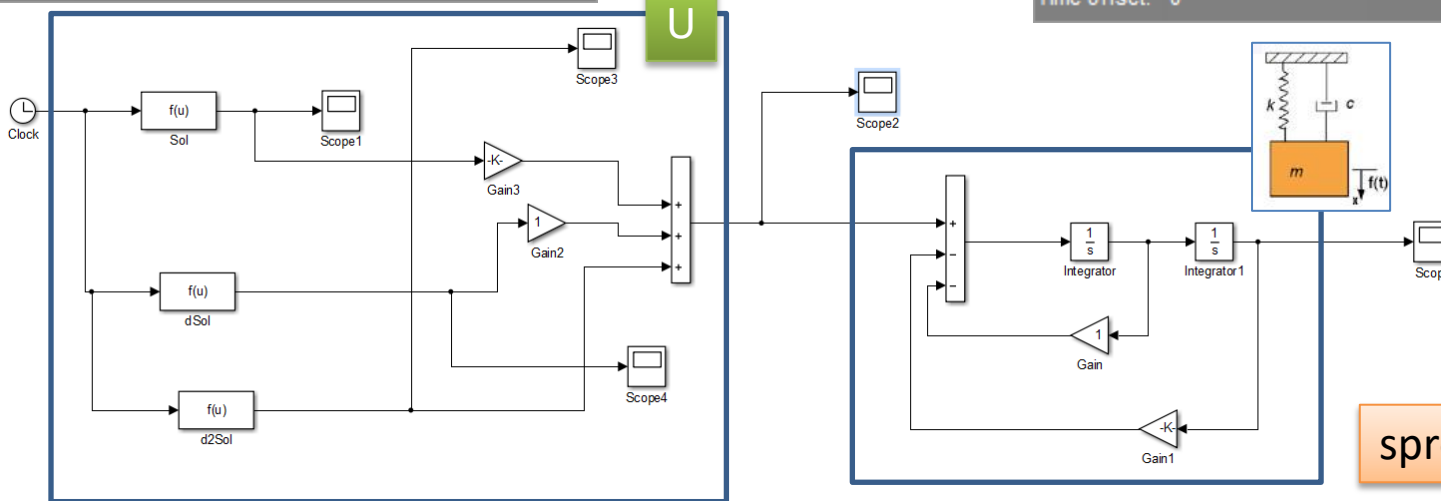
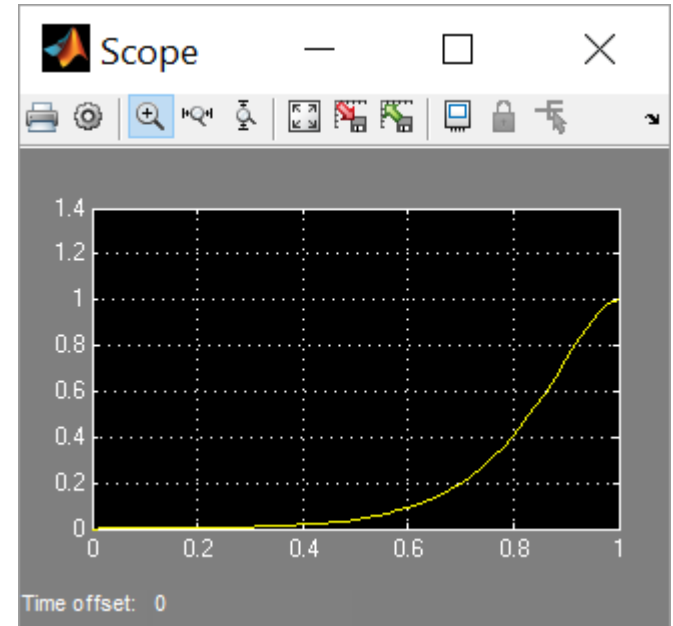
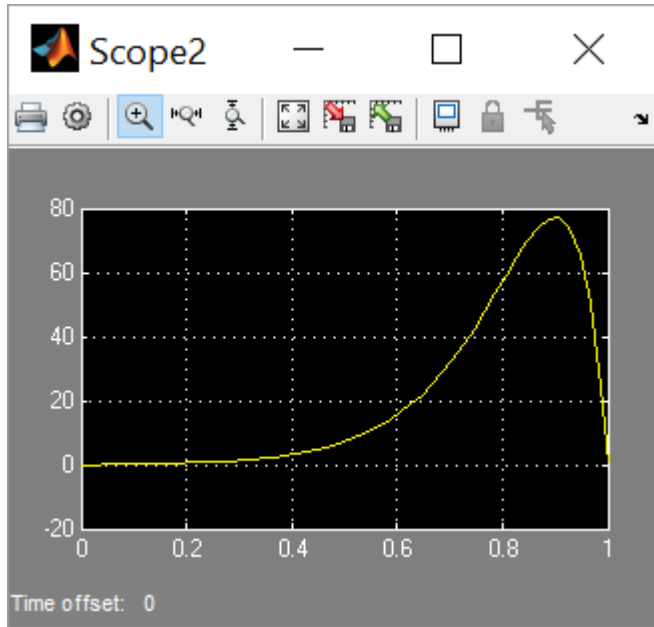


# Sterowanie optymalne

$$\frac{d^2x(t)}{dt^2} + c \frac{dx(t)}{dt} + Kx(t) = u(t)$$

$m=1\text{kg};$   
 $c=1\text{kg/s};$   
 $K=100\text{kg/s}^2;$

$t_1=0;$   
 $x_1=0;$   
 $dx_1=0;$   
 $t_2=1;$   
 $x_2=1;$   
 $dx_2=0;$



sprezynaOpt.slx

# Zagadnienie

$$\frac{d^n x(t)}{dt^n} = u(t)$$

$$x^{(n)} = u$$

$$J = \int_0^T [u(t)]^2 dt = \int_0^T [x^{(n)}(t)]^2 dt$$

$$F_x - \frac{d}{dt} F_{\dot{x}} + \frac{d^2}{dt^2} F_{\ddot{x}} + \dots + (-1)^n \frac{d^n}{dt^n} F_{x^{(n)}} = 0,$$

$$F = [x^{(n)}(t)]^2$$

$$F_x = F_{\dot{x}} = F_{\ddot{x}} = \dots = F_{x^{(n-1)}} = 0,$$

$$\frac{d^{2n} x(t)}{dt^{2n}} = 0,$$

$$x(t) = C_0 + C_1 t + \dots + C_{2n-1} t^{2n-1}.$$

$$u = \sum_{i=1}^n q_{i-1} t^{i-1}.$$

# Przykład

$$\frac{d^3 x(t)}{dt^3} = u(t) \Rightarrow J = \int_0^T [u(t)]^2 dt = \int_0^T [x^{(n)}(t)]^2 dt \Rightarrow J = \int_0^T [x^{(3)}(t)]^2 dt$$

$$x_1(0) = x(0) = 1, \quad x_2(0) = \dot{x}(0) = 1, \quad x_3(0) = \ddot{x}(0) = 1;$$

$$x_1(T) = x(T) = 0,5, \quad x_2(T) = \dot{x}(T) = 0, \quad x_3(T) = \ddot{x}(T) = 0;$$

$$T = 5 \text{ s.}$$

$$\cancel{F_x} - \cancel{\frac{d}{dt} F_{\dot{x}}} + \cancel{\frac{d^2}{dt^2} F_{\ddot{x}}} + \dots + (-1)^n \frac{d^n}{dt^n} F_{x^{(n)}} = \mathbf{0},$$

$$F_{\ddot{x}} = 2\ddot{x}$$

$$\frac{d^3(\ddot{x})}{dt^3} = x^{(6)}$$

# Rozwiązanie

$$\frac{d^{2n} x(t)}{dt^{2n}} = 0,$$

$$\frac{d^6 x(t)}{dt^6} = 0.$$

```
>> x1 = dsolve('D6x1=0')
```

```
x1 =
```

```
1/120*C1*t^5+1/24*C2*t^4+1/6*C3*t^3+1/2*C4*t^2+C5*t+C6
```

$$x_1(t) = x(t) = \frac{C_1}{120} t^5 + \frac{C_2}{24} t^4 + \frac{C_3}{6} t^3 + \frac{C_4}{2} t^2 + C_5 t + C_6.$$

# Obliczenie stałych

```
>> x2 = dsolve('D5x2=0')
```

```
x2 =
```

```
1/24*C1*t^4+1/6*C2*t^3+1/2*C3*t^2+C4*t+C5
```

```
>> x3 = dsolve('D4x3=0')
```

```
x3 =
```

```
1/6*C1*t^3+1/2*C2*t^2+C3*t+C4
```

$$x_2(t) = \dot{x}(t) = \frac{C_1}{24}t^4 + \frac{C_2}{6}t^3 + \frac{1}{2}C_3t^2 + C_4t + C_5;$$

$$x_3(t) = \ddot{x}(t) = \frac{C_1}{6}t^3 + \frac{C_2}{2}t^2 + C_3t + C_4.$$

$$\left\{ \begin{array}{l} x_1(0) = C_6; \\ x_2(0) = C_5; \\ x_3(0) = C_4; \\ x_1(T) = \frac{C_1}{120}T^5 + \frac{C_2}{24}T^4 + \frac{C_3}{6}T^3 + \frac{C_4}{2}T^2 + C_5T + C_6; \\ x_2(T) = \frac{C_1}{24}T^4 + \frac{C_2}{6}T^3 + \frac{C_3}{2}T^2 + C_4T + C_5; \\ x_3(T) = \frac{C_1}{6}T^3 + \frac{C_2}{2}T^2 + C_3T + C_4. \end{array} \right.$$

# Rozwiązanie systemu

```
>> syms c1 c2 c3 c4 c5 c6
%warunki końcowe
x10=1; x20=1; x30=1;
x1T=0.5; x2T=0; x3T=0;
T=5;
%system równań algebraicznych
eq1=c6-x10;
eq2=c5-x20;
eq3=c4-x30;
eq4=c1/120*T^5+c2/24*T^4+c3/6*T^3+c4/2*T^2+c5*T+c6-x1T;
eq5=c1/24*T^4+c2/6*T^3+c3/2*T^2+c4*T+c5-x2T;
eq6=c1/6*T^3+c2/2*T^2+c3*T+c4-x3T;
%rozwiązanie
[c1,c2,c3,c4,c5,c6]= solve(eq1, eq2, eq3, eq4, eq5, eq6)
```

$$C_1 = -1,1712; C_2 = 3,2640; C_3 = -3,4800; C_4 = 1; C_5 = 1; C_6 = 1.$$

# Sposób drugi

$$\mathbf{x} = \mathbf{A}\mathbf{c} \quad \mathbf{c} = \mathbf{A}^{-1}\mathbf{x}$$

$$\mathbf{A} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ \frac{T^5}{120} & \frac{T^4}{24} & \frac{T^3}{6} & \frac{T^2}{2} & T & 1 \\ \frac{T^4}{24} & \frac{T^3}{6} & \frac{T^2}{2} & T & 1 & 0 \\ \frac{T^3}{6} & \frac{T^2}{2} & T & 1 & 0 & 0 \end{bmatrix}; \mathbf{x} = \begin{bmatrix} x_1(0) \\ x_2(0) \\ x_3(0) \\ x_1(T) \\ x_2(T) \\ x_3(T) \end{bmatrix} = \begin{bmatrix} x(0) \\ \dot{x}(0) \\ \ddot{x}(0) \\ x(T) \\ \dot{x}(T) \\ \ddot{x}(T) \end{bmatrix}.$$



# Macierz odwrotna

```
>> syms c1 c2 c3 c4 c5 c6
%warunki końcowe i macierz
x10=1; x20=1; x30=1;
x1T=0.5; x2T=0; x3T=0;
T=5;
x=[ x10; x20; x30; x1T; x2T; x3T];
A=[0 0 0 0 0 1; 0 0 0 0 1 0; 0 0 0 1 0 0;
T^5/120 T^4/24 T^3/6 T^2/2 T 1;
T^4/24 T^3/6 T^2/2 T 1 0; T^3/6 T^2/2 T 1
0 0];
%rozwiązanie
c=inv(A)*x
```

# Sterowanie optymalne

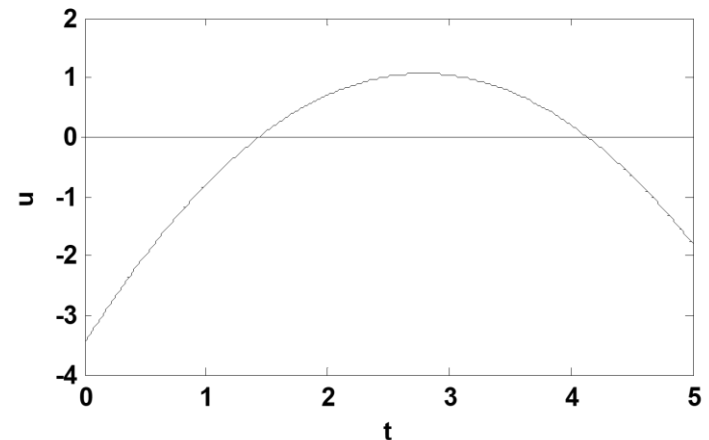
$$\frac{d^3 x(t)}{dt^3} = u(t)$$

$$\ddot{x}(t) = \frac{C_1}{2}t^2 + C_2t + C_3. \quad u(t) = \ddot{x}(t) = q_0 + q_1t + q_2t^2,$$

$$q_0 = C_3 = -3,4800; q_1 = C_2 = 3,2640; q_2 = C_1/2 = -0,5856.$$

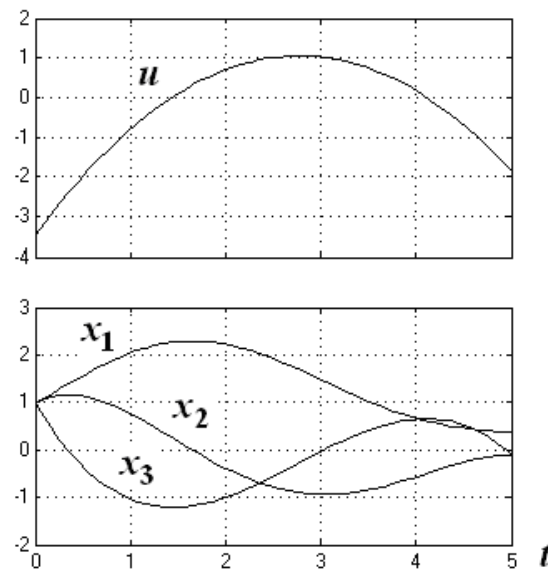
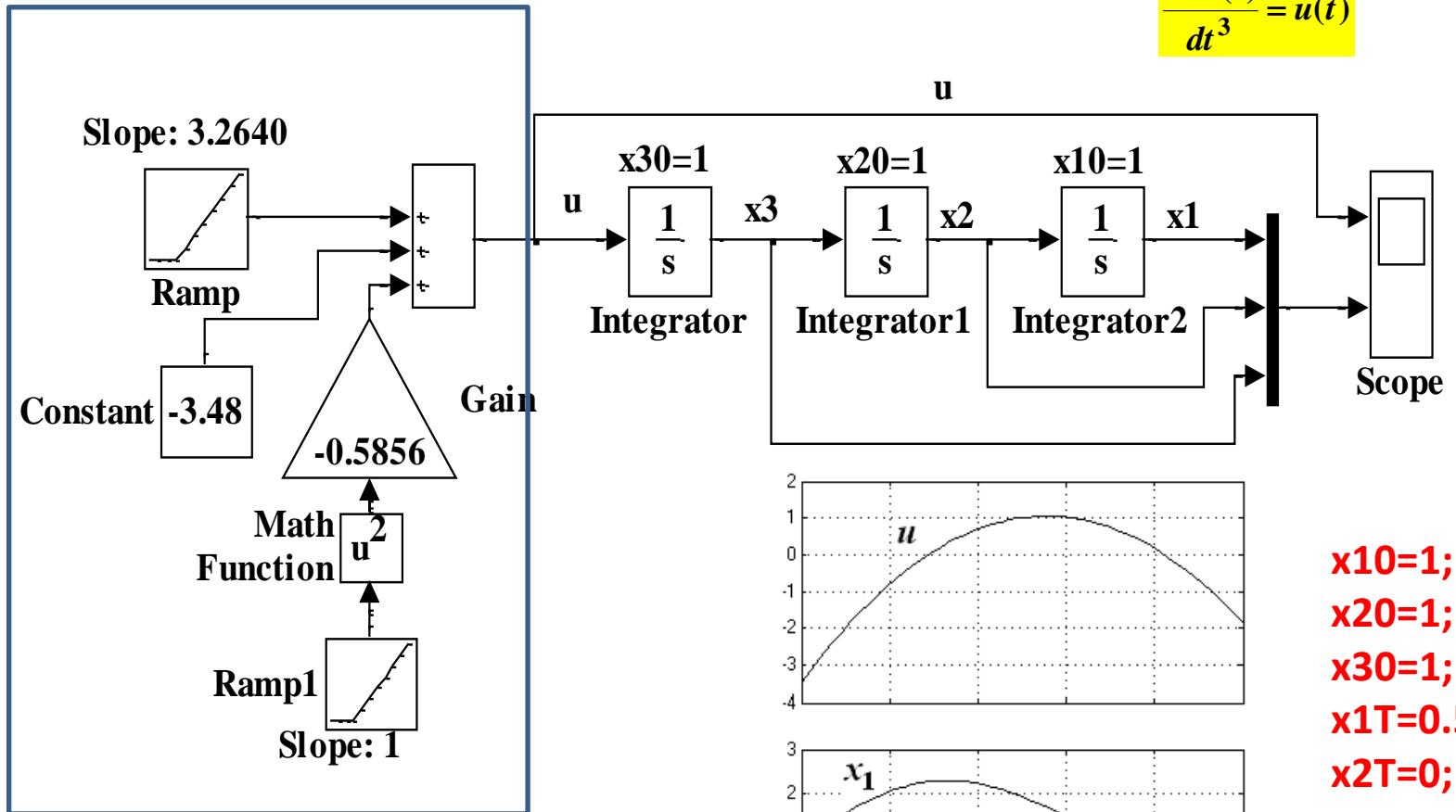
$$u(t) = -3,4800 + 3,2640t - 0,5856t^2.$$

```
>>t=0:0.01:5;  
u=-3.4800+3.2640*t-0.5856*t.^2;  
plot(t,u)  
xlabel('t'), ylabel('u')
```



# Symulacja

$$\frac{d^3 x(t)}{dt^3} = u(t)$$



- $x_{10}=1;$**
- $x_{20}=1;$**
- $x_{30}=1;$**
- $x_{1T}=0.5;$**
- $x_{2T}=0;$**
- $x_{3T}=0;$**
- $T=5;$**

# Przykład

$$W(s) = \frac{X(s)}{U(s)} = \frac{1}{s^2(\tau s + 1)}, \quad J = \int_0^T F dt = \int_0^T u^2(t) dt = \int_0^T (\tau \ddot{x} + \dot{x})^2 dt.$$

$$\tau \ddot{x}(t) + \dot{x}(t) = u(t)$$

$$\dot{x}_1 = x_2;$$

$$x_1 = x$$

$$\dot{x}_2 = x_3;$$

$$\dot{x}_3 = -\frac{1}{\tau} x_3 + \frac{1}{\tau} u,$$

$$x_1(0) = x(0) = 1, \quad x_2(0) = \dot{x}(0) = 0, \quad x_3(0) = \ddot{x}(0) = 0;$$

$$x_1(T) = x(T) = 0, \quad x_2(T) = \dot{x}(T) = 0, \quad x_3(T) = \ddot{x}(T) = 0;$$

$$\tau = 1 \text{ s}; T = 2 \text{ s}.$$

# Rozwiązanie

$$F_x - \frac{d}{dt} F_{\dot{x}} + \frac{d^2}{dt^2} F_{\ddot{x}} - \frac{d^3}{dt^3} F_{\ddot{x}} = 0.$$

$$F = (\tau \ddot{x} + \ddot{x})^2; F_x = \frac{\partial F}{\partial x} = 0; F_{\dot{x}} = \frac{\partial F}{\partial \dot{x}} = 0;$$

$$F_{\ddot{x}} = \frac{\partial F}{\partial \ddot{x}} = 2(\tau \ddot{x} + \ddot{x}); F_{\ddot{x}} = \frac{\partial F}{\partial \ddot{x}} = 2\tau (\tau \ddot{x} + \ddot{x}).$$

$$2(\tau x^{(5)} + x^{(4)}) - 2\tau (\tau x^{(6)} + x^{(5)}) = 0,$$

$$\tau^2 x^{(6)} - x^{(4)} = 0.$$

# Rozwiązanie

```
>> x = dsolve('tau^2*D6x-D4x=0')
```

x =

```
C1+C2*t+C3*t^2+C4*t^3+C5*exp(-1/tau*t)+C6*exp(1/tau*t)
```

$$x(t) = C_1 + C_2 t + C_3 t^2 + C_4 t^3 + C_5 e^{-\frac{t}{\tau}} + C_6 e^{\frac{t}{\tau}}.$$

$$\dot{x}(t) = C_2 + 2C_3 t + 3C_4 t^2 - \frac{1}{\tau} C_5 e^{-\frac{t}{\tau}} + \frac{1}{\tau} C_6 e^{\frac{t}{\tau}};$$

$$\ddot{x}(t) = 2C_3 + 6C_4 t + \frac{1}{\tau^2} C_5 e^{-\frac{t}{\tau}} + \frac{1}{\tau^2} C_6 e^{\frac{t}{\tau}}.$$

# Rozwiązanie

$$\left\{ \begin{array}{l} x_1(0) = C_1 + C_2 + C_6; \\ x_2(0) = C_2 - \frac{1}{\tau}C_5 + \frac{1}{\tau}C_6; \\ x_3(0) = 2C_3 + \frac{1}{\tau^2}C_5 + \frac{1}{\tau^2}C_6; \\ x_1(T) = C_1 + C_2T + C_3T^2 + C_4T^3 + C_5e^{-\frac{T}{\tau}} + C_6e^{\frac{T}{\tau}}; \\ x_2(T) = C_2 + 2C_3T + 3C_4T^2 - \frac{1}{\tau}C_5e^{-\frac{T}{\tau}} + \frac{1}{\tau}C_6e^{\frac{T}{\tau}}; \\ x_3(T) = 2C_3 + 6C_4T + \frac{1}{\tau^2}C_5e^{-\frac{T}{\tau}} + \frac{1}{\tau^2}C_6e^{\frac{T}{\tau}}. \end{array} \right.$$

# Reguła sterowania

$$\ddot{x}(t) = 6C_4 - \frac{1}{\tau^3} C_5 e^{-\frac{t}{\tau}} + \frac{1}{\tau^3} C_6 e^{\frac{t}{\tau}}.$$

$$u(t) = \tau \ddot{x}(t) + \dot{x}(t) = \tau \left( 6C_4 - \frac{1}{\tau^3} C_5 e^{-\frac{t}{\tau}} + \frac{1}{\tau^3} C_6 e^{\frac{t}{\tau}} \right) +$$

$$+ 2C_3 + 6C_4 t + \frac{1}{\tau^2} C_5 e^{-\frac{t}{\tau}} + \frac{1}{\tau^2} C_6 e^{\frac{t}{\tau}} =$$

$$= 2C_3 + 6C_4 \tau + 6C_4 t + 2 \frac{1}{\tau^2} C_6 e^{\frac{t}{\tau}},$$

$$q_0 = 2C_3 + 6C_4 \tau; \quad q_1 = 6C_4; \quad q_2 = 2 \frac{1}{\tau^2} C_6.$$

$$u(t) = q_0 + q_1 t + q_2 e^{\frac{t}{\tau}},$$

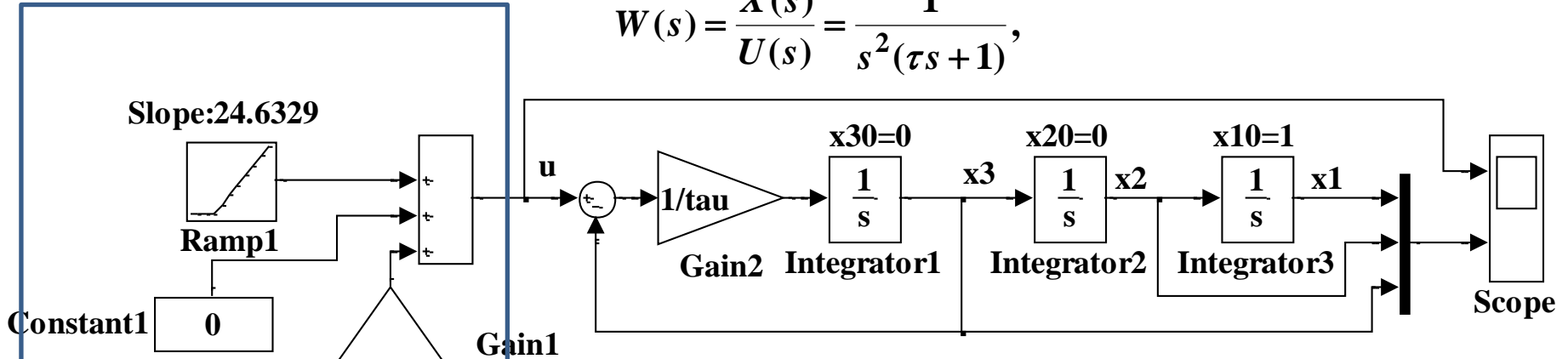


# Program

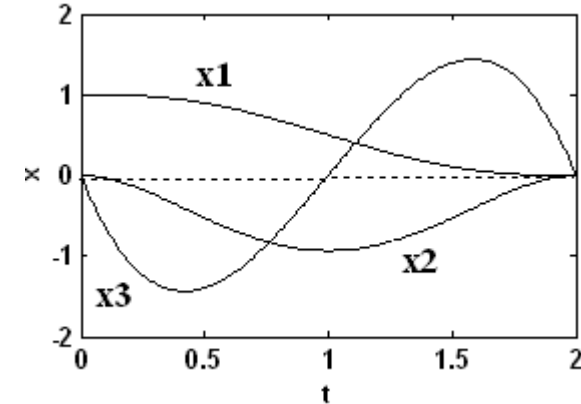
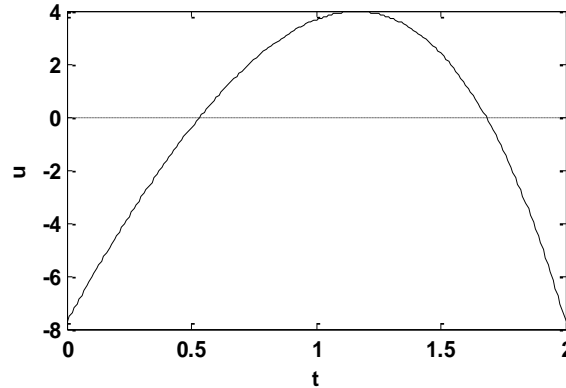
```
>> syms c1 c2 c3 c4 c5 c6
tau=1; T=2;
x10=1; x20=0; x30=0;
x1T=0; x2T=0; x3T=0;
eq1=c1+c5+c6-x10;
eq2=c2-1/tau*c5+1/tau*c6-x20;
eq3=2*c3+1/tau^2*c5+1/tau^2*c6-x30;
eq4=c1+c2*T+c3*T^2+c4*T^3+c5*exp(-
T/tau)+c6*exp(T/tau)-x1T;
eq5= c2 +2*c3*T+3*c4*T^2-1/tau*c5*exp(-
T/tau)+1/tau*c6*exp(T/tau)-x2T;
eq6= 2*c3 +6*c4*T+1/tau^2*c5*exp(-
T/tau)+1/tau^2*c6*exp(T/tau)-x3T;
[c1,c2,c3,c4,c5,c6]= solve(eq1, eq2, eq3, eq4,
eq5, eq6)
c1 =
-23.6329
c2 =
32.3439
c3 =
-12.3165
c4 =
4.1055
c5 =
28.4884
c6 =
-3.8555
q0=2*c3+6*c4*tau;
q1=6*c4;
q2=2/tau^2*c6;
[q0], [q1], [q2]
q0 =
0
q1 =
24.6329
q2 =
-7.7110
```

# Model

$$W(s) = \frac{X(s)}{U(s)} = \frac{1}{s^2(\tau s + 1)},$$

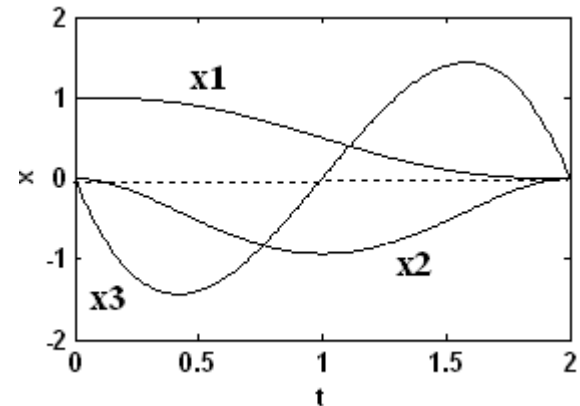
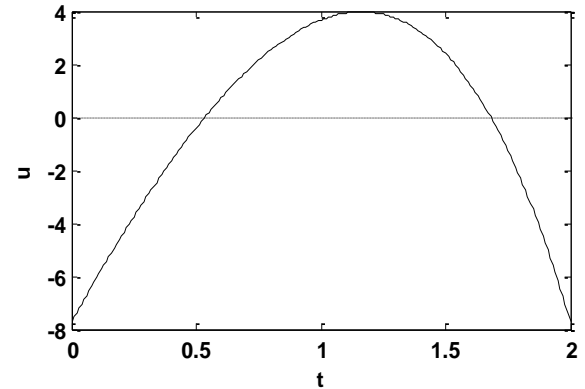


Simulation time  
Start time: 0.0 Stop time: 2



# Analiza

```
>> x1=c1+c2*t+c3*t.^2+c4*t.^3+c5*exp(-  
1./tau*t)+c6*exp(1./tau*t);  
plot(t,x1, 'k -')  
hold on  
x2= c2 +2*c3*t+3*c4*t.^2-1/tau*c5*exp(-  
1./tau*t)+1/tau*c6*exp(1./tau*t);  
plot(t,x2, 'k-')  
hold on  
x3= 2*c3 +6*c4*t+1/tau^2*c5*exp(-  
1./tau*t)+1/tau^2*c6*exp(1./tau*t);  
plot(t,x3, 'k-')  
xlabel('t'), ylabel('x')
```



# Oscylator harmoniczny tłumiony (2)

$$W(s) = \frac{X(s)}{U(s)} = \frac{\omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

$$\ddot{x}(t) + 2\xi\omega_0\dot{x}(t) + \omega_0^2x(t) = \omega_0^2u(t),$$

$$x_1(0) = x(0) = 1, \quad x_2(0) = \dot{x}(0) = 1;$$

$$x_1(T) = x(T) = 0, \quad x_2(T) = \dot{x}(T) = 0;$$

$$\xi = 0,1; \omega_0 = 0,5 \text{ s}^{-1}; T = 5 \text{ s}.$$

$$J = \int_0^T F dt = \int_0^T u^2(t) dt = \int_0^T [(\ddot{x} + 2\xi\omega_0\dot{x} + \omega_0^2x) / \omega_0^2]^2 dt,$$

# Układ dynamiczny II rzędu

Układ dynamiczny II rzędu - układ dynamiczny opisany równaniem:

$$a_2 \frac{d^2 y(t)}{dt^2} + a_1 \frac{dy(t)}{dt} + a_0 y(t) = u(t)$$

Jego transmitancja dana jest wzorem:

$$G(s) = \frac{1}{a_2(s^2 + 2\tau s + \gamma^2)}$$

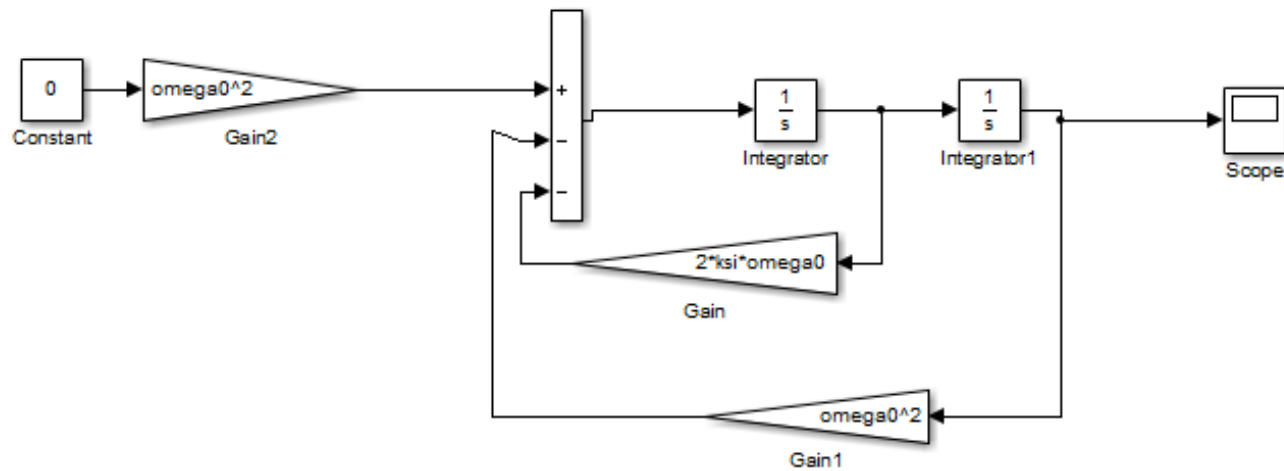
gdzie:

$$2\tau = \frac{a_1}{a_2}, \gamma^2 = \frac{a_0}{a_2}$$

Gdy:

- $\tau^2 > \gamma^2$ , jest to **układ przetłumiony**
- $\tau^2 = \gamma^2$ , jest to **układ tłumiony krytycznie**
- $\tau^2 < \gamma^2$ , jest to **układ niedotłumiony**

# Symulacja

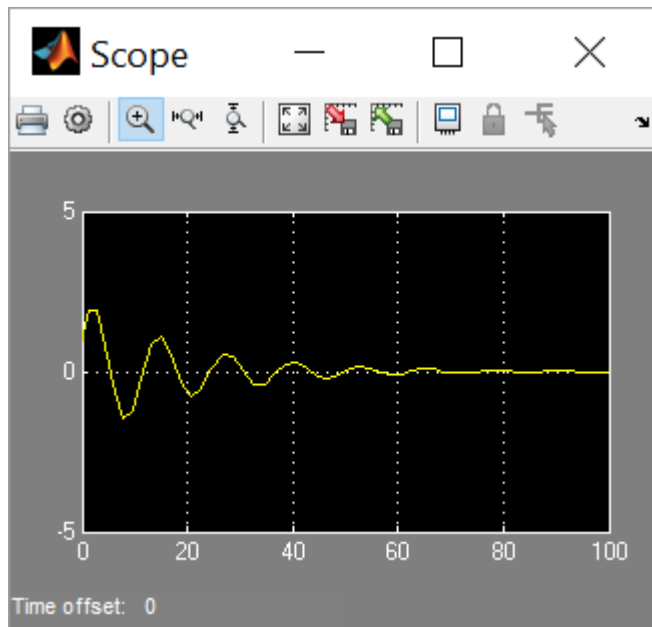


$$\begin{aligned}x_1(0) &= x(0) = 1, & x_2(0) &= \dot{x}(0) = 1; \\x_1(T) &= x(T) = 0, & x_2(T) &= \dot{x}(T) = 0; \\ \xi &= 0,1; & \omega_0 &= 0,5 \text{ s}^{-1}; & T &= 5 \text{ s}.\end{aligned}$$

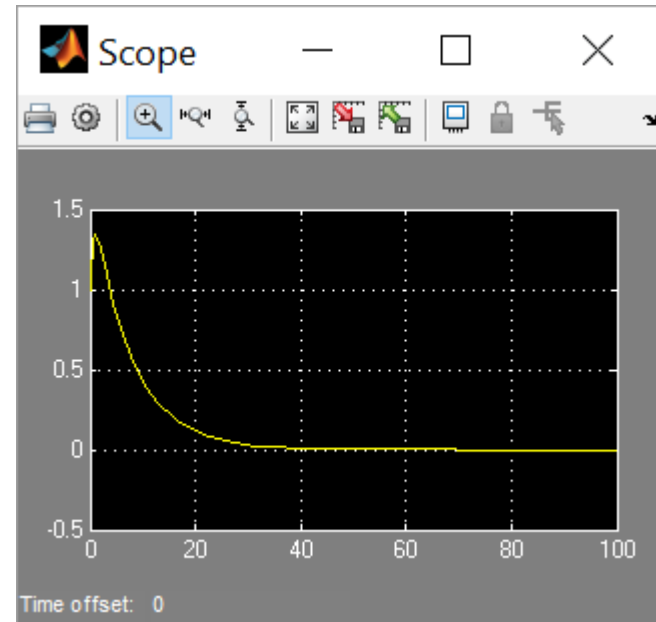
sprezynaKsiOmega.slx

# Tłumienie

Ksi=0.1



Ksi=2



# Rozwiązanie

$$F = [(\ddot{x} + 2\xi\omega_0\dot{x} + \omega_0^2x) / \omega_0^2]^2.$$

$$F_x - \frac{d}{dt}F_{\dot{x}} + \frac{d^2}{dt^2}F_{\ddot{x}} + \dots + (-1)^n \frac{d^n}{dt^n}F_{x^{(n)}} = 0,$$

$$n = 2$$

$$F_x - \frac{d}{dt}F_{\dot{x}} + \frac{d^2}{dt^2}F_{\ddot{x}} = 0.$$



# Obliczenia w MatLabie

```
>> syms ksi omega0 x xdot xdotdot
F=((xdotdot+2*ksi*omega0*xdot+omega0^2*x)/omega0^2)^2;
Fx=diff(F,'x')
Fxdot=diff(F,'xdot')
Fxdotdot=diff(F,'xdotdot')

Fx = 2*(xdotdot+2*ksi*omega0*xdot+omega0^2*x)/omega0^2
Fxdot = 4*(xdotdot+2*ksi*omega0*xdot+omega0^2*x)/omega0^3*ksi
Fxdotdot = 2*(xdotdot+2*ksi*omega0*xdot+omega0^2*x)/omega0^4
```

$$F_x = \frac{\partial F}{\partial x} = 2(\ddot{x} + 2\xi\omega_0\dot{x} + \omega_0^2x) / \omega_0^2,$$
$$F_{\dot{x}} = \frac{\partial F}{\partial \dot{x}} = 4\xi(\ddot{x} + 2\xi\omega_0\dot{x} + \omega_0^2x) / \omega_0^3,$$
$$F_{\ddot{x}} = \frac{\partial F}{\partial \ddot{x}} = 2(\ddot{x} + 2\xi\omega_0\dot{x} + \omega_0^2x) / \omega_0^4.$$

$$\frac{d}{dt} F_{\dot{x}} = 4\xi(\ddot{x} + 2\xi\omega_0\dot{x} + \omega_0^2x) / \omega_0^3;$$
$$\frac{d^2}{dt^2} F_{\ddot{x}} = 2(x^{(4)} + 2\xi\omega_0\ddot{x} + \omega_0^2\ddot{x}) / \omega_0^4.$$

# Równanie Eulera-Poissona

$$2(\ddot{x} + 2\xi\omega_0\dot{x} + \omega_0^2x)/\omega_0^2 - 4\xi(\ddot{x} + 2\xi\omega_0\dot{x} + \omega_0^2x)/\omega_0^3 + \\ + 2(x^{(4)} + 2\xi\omega_0\ddot{x} + \omega_0^2\ddot{x})/\omega_0^4 = 0,$$

lub

$$x^{(4)} + 2\omega_0^2(1 - 2\xi^2)\ddot{x} + \omega_0^4x = 0.$$

```
>> x = dsolve('D4x+2*omega0^2*(1-2*ksi^2)*D2x+omega0^4*x=0');
pretty(x)
```

```
C1 exp((-ksi + (ksi - 1)^(1/2)) omega0 t)
+ C2 exp(-(ksi + (ksi - 1)^(1/2)) omega0 t)
+ C3 exp((ksi + (ksi - 1)^(1/2)) omega0 t)
+ C4 exp(-(-ksi + (ksi - 1)^(1/2)) omega0 t)
```

$$x = C_1 e^{\left(-\xi\omega_0 + \omega_0\sqrt{\xi^2 - 1}\right)t} + C_2 e^{-\left(\xi\omega_0 + \omega_0\sqrt{\xi^2 - 1}\right)t} + \\ + C_3 e^{\left(\xi\omega_0 + \omega_0\sqrt{\xi^2 - 1}\right)t} + C_4 e^{-\left(-\xi\omega_0 + \omega_0\sqrt{\xi^2 - 1}\right)t}.$$

# Rozwiązanie

$$x = e^{-\xi\omega_0 t} \left( C_1 e^{j\omega_0 \sqrt{1-\xi^2} t} + C_2 e^{-j\omega_0 \sqrt{1-\xi^2} t} \right) + e^{\xi\omega_0 t} \left( C_3 e^{j\omega_0 \sqrt{1-\xi^2} t} + C_4 e^{-j\omega_0 \sqrt{1-\xi^2} t} \right).$$

$$\xi < 1$$

$$x = e^{-\xi\omega_0 t} (C_1 \sin \omega_0 \sqrt{1-\xi^2} t + C_2 \cos \omega_0 \sqrt{1-\xi^2} t) + e^{\xi\omega_0 t} (C_3 \sin \omega_0 \sqrt{1-\xi^2} t + C_4 \cos \omega_0 \sqrt{1-\xi^2} t).$$

Uklad2ksiM1.m

# Wyniki obliczenia

$\dot{x}$  =

$$-\omega_0 \kappa \exp(-\omega_0 \kappa t) (C_1 \sin(\omega_0 (1-\kappa^2)^{1/2} t) + C_2 \cos(\omega_0 (1-\kappa^2)^{1/2} t)) + \exp(-\omega_0 \kappa t) (C_1 \cos(\omega_0 (1-\kappa^2)^{1/2} t) \omega_0 (1-\kappa^2)^{1/2} - C_2 \sin(\omega_0 (1-\kappa^2)^{1/2} t) \omega_0 (1-\kappa^2)^{1/2}) + \omega_0 \kappa \exp(\omega_0 \kappa t) (C_3 \sin(\omega_0 (1-\kappa^2)^{1/2} t) + C_4 \cos(\omega_0 (1-\kappa^2)^{1/2} t)) + \exp(\omega_0 \kappa t) (C_3 \cos(\omega_0 (1-\kappa^2)^{1/2} t) \omega_0 (1-\kappa^2)^{1/2} - C_4 \sin(\omega_0 (1-\kappa^2)^{1/2} t) \omega_0 (1-\kappa^2)^{1/2})$$

$\ddot{x}$  =

$$\omega_0^2 \kappa^2 \exp(-\omega_0 \kappa t) (C_1 \sin(\omega_0 (1-\kappa^2)^{1/2} t) + C_2 \cos(\omega_0 (1-\kappa^2)^{1/2} t)) - 2 \omega_0 \kappa \exp(-\omega_0 \kappa t) (C_1 \cos(\omega_0 (1-\kappa^2)^{1/2} t) \omega_0 (1-\kappa^2)^{1/2} - C_2 \sin(\omega_0 (1-\kappa^2)^{1/2} t) \omega_0 (1-\kappa^2)^{1/2}) + \exp(-\omega_0 \kappa t) (-C_1 \sin(\omega_0 (1-\kappa^2)^{1/2} t) \omega_0^2 (1-\kappa^2) - C_2 \cos(\omega_0 (1-\kappa^2)^{1/2} t) \omega_0^2 (1-\kappa^2)) + \omega_0^2 \kappa^2 \exp(\omega_0 \kappa t) (C_3 \sin(\omega_0 (1-\kappa^2)^{1/2} t) + C_4 \cos(\omega_0 (1-\kappa^2)^{1/2} t)) + 2 \omega_0 \kappa \exp(\omega_0 \kappa t) (C_3 \cos(\omega_0 (1-\kappa^2)^{1/2} t) \omega_0 (1-\kappa^2)^{1/2} - C_4 \sin(\omega_0 (1-\kappa^2)^{1/2} t) \omega_0 (1-\kappa^2)^{1/2}) + \exp(\omega_0 \kappa t) (-C_3 \sin(\omega_0 (1-\kappa^2)^{1/2} t) \omega_0^2 (1-\kappa^2) - C_4 \cos(\omega_0 (1-\kappa^2)^{1/2} t) \omega_0^2 (1-\kappa^2))$$

# Wyznaczenie współczynników

$$C_1, C_2, C_3, C_4$$

$$x_1(0) = x(0) = 1, \quad x_2(0) = \dot{x}(0) = 1;$$

$$x_1(T) = x(T) = 0, \quad x_2(T) = \dot{x}(T) = 0;$$

$$\xi = 0,1; \omega_0 = 0,5 \text{ s}^{-1}; T = 5 \text{ s}.$$

```
syms ksi omega0 C1 C2 C3 C4 t
% wprowadzenie x
x=exp(-ksi*omega0*t)*(C1*sin(omega0*sqrt(1-
ksi^2)*t)+C2*cos(omega0*sqrt(1-
ksi^2)*t))+exp(ksi*omega0*t)*(C3*sin(omega0*sqrt(1-
ksi^2)*t)+C4*cos(omega0*sqrt(1-ksi^2)*t));
xdot=diff(x,'t')
xdotdot= diff(xdot,'t')
```

# Układ równań

>> **t=0;**

```
x0=exp(-ksi*omega0*t)*(C1*sin(omega0*sqrt(1-ksi^2)*t)+C2*cos(omega0*sqrt(1-ksi^2)*t))+exp(ksi*omega0*t)*(C3*sin(omega0*sqrt(1-ksi^2)*t)+C4*cos(omega0*sqrt(1-ksi^2)*t))
```

$$x_0 = C_2 + C_4$$

```
xdot0=-omega0*ksi*exp(-omega0*ksi*t)*(C1*sin(omega0*(1-ksi^2)^(1/2)*t)+C2*cos(omega0*(1-ksi^2)^(1/2)*t))+exp(-omega0*ksi*t)*(C1*cos(omega0*(1-ksi^2)^(1/2)*t)*omega0*(1-ksi^2)^(1/2)-C2*sin(omega0*(1-ksi^2)^(1/2)*t)*omega0*(1-ksi^2)^(1/2))+omega0*ksi*exp(omega0*ksi*t)*(C3*sin(omega0*(1-ksi^2)^(1/2)*t)+C4*cos(omega0*(1-ksi^2)^(1/2)*t))+exp(omega0*ksi*t)*(C3*cos(omega0*(1-ksi^2)^(1/2)*t)*omega0*(1-ksi^2)^(1/2)-C4*sin(omega0*(1-ksi^2)^(1/2)*t)*omega0*(1-ksi^2)^(1/2))
```

$$\dot{x}_0 = -\omega_0 \text{ksi} C_2 + C_1 \omega_0 (1 - \text{ksi}^2)^{1/2} + \omega_0 \text{ksi} C_4 + C_3 \omega_0 (1 - \text{ksi}^2)^{1/2}$$

>> **syms T**

```
xT=exp(-ksi*omega0*T)*(C1*sin(omega0*sqrt(1-ksi^2)*T)+C2*cos(omega0*sqrt(1-ksi^2)*T))+exp(ksi*omega0*T)*(C3*sin(omega0*sqrt(1-ksi^2)*T)+C4*cos(omega0*sqrt(1-ksi^2)*T));
```

```
>>xdotT=-omega0*ksi*exp(-omega0*ksi*T)*(C1*sin(omega0*(1-ksi^2)^(1/2)*T)+C2*cos(omega0*(1-ksi^2)^(1/2)*T))+exp(-omega0*ksi*T)*(C1*cos(omega0*(1-ksi^2)^(1/2)*T)*omega0*(1-ksi^2)^(1/2)-C2*sin(omega0*(1-ksi^2)^(1/2)*T)*omega0*(1-ksi^2)^(1/2))+omega0*ksi*exp(omega0*ksi*T)*(C3*sin(omega0*(1-ksi^2)^(1/2)*T)+C4*cos(omega0*(1-ksi^2)^(1/2)*T))+exp(omega0*ksi*T)*(C3*cos(omega0*(1-ksi^2)^(1/2)*T)*omega0*(1-ksi^2)^(1/2)-C4*sin(omega0*(1-ksi^2)^(1/2)*T)*omega0*(1-ksi^2)^(1/2))
```

# Rozwiązanie systemu równań

```
T=5;
ksi=0.1; omega0=0.5;
x0=1; xdot0=1; xT=0; xdotT=0;
eq1= C2+C4-x0;
eq2=-omega0*ksi*C2+C1*omega0*(1-ksi^2)^(1/2)+omega0*ksi*C4+C3*omega0*(1-ksi^2)^(1/2)-xdot0;
eq3=exp(-ksi*omega0*T)*(C1*sin(omega0*sqrt(1-ksi^2)*T)+C2*cos(omega0*sqrt(1-ksi^2)*T))+exp(ksi*omega0*T)*(C3*sin(omega0*sqrt(1-ksi^2)*T)+C4*cos(omega0*sqrt(1-ksi^2)*T))-xT;
eq4=-omega0*ksi*exp(-omega0*ksi*T)*(C1*sin(omega0*(1-ksi^2)^(1/2)*T)+C2*cos(omega0*(1-ksi^2)^(1/2)*T))+exp(-omega0*ksi*T)*(C1*cos(omega0*(1-ksi^2)^(1/2)*T)*omega0*(1-ksi^2)^(1/2)-C2*sin(omega0*(1-ksi^2)^(1/2)*T)*omega0*(1-ksi^2)^(1/2))+omega0*ksi*exp(omega0*ksi*T)*(C3*sin(omega0*(1-ksi^2)^(1/2)*T)+C4*cos(omega0*(1-ksi^2)^(1/2)*T))+exp(omega0*ksi*T)*(C3*cos(omega0*(1-ksi^2)^(1/2)*T)*omega0*(1-ksi^2)^(1/2)-C4*sin(omega0*(1-ksi^2)^(1/2)*T)*omega0*(1-ksi^2)^(1/2))- xdotT;
```

```
[C1,C2,C3,C4]= solve(eq1, eq2, eq3, eq4)
```

```
C1 =
```

```
6.7790
```

```
C2 =
```

```
2.8872
```

```
C3 =
```

```
-4.2890
```

```
C4 =
```

```
-1.8872
```

# Symulacja

T=5;  
ksi=0.1; omega0=0.5; C1 =6.7790; C2 =2.8872; C3 =-4.2890;  
C4 =-1.8872;  
**t=0:0.01:5;**

```
x=exp(-ksi*omega0*t).*(C1*sin(omega0*sqrt(1-ksi^2)*t)+C2*cos(omega0*sqrt(1-ksi^2)*t))+exp(ksi*omega0*t).*(C3*sin(omega0*sqrt(1-ksi^2)*t)+C4*cos(omega0*sqrt(1-ksi^2)*t));  
xdot=-omega0*ksi*exp(-omega0*ksi*t).*(C1*sin(omega0*(1-ksi^2)^(1/2)*t)+C2*cos(omega0*(1-ksi^2)^(1/2)*t))+exp(-omega0*ksi*t).*(C1*cos(omega0*(1-ksi^2)^(1/2)*t)*omega0*(1-ksi^2)^(1/2)-C2*sin(omega0*(1-ksi^2)^(1/2)*t)*omega0*(1-ksi^2)^(1/2))+omega0*ksi*exp(omega0*ksi*t).*(C3*sin(omega0*(1-ksi^2)^(1/2)*t)+C4*cos(omega0*(1-ksi^2)^(1/2)*t))+exp(omega0*ksi*t).*(C3*cos(omega0*(1-ksi^2)^(1/2)*t)*omega0*(1-ksi^2)^(1/2)-C4*sin(omega0*(1-ksi^2)^(1/2)*t)*omega0*(1-ksi^2)^(1/2));  
xdotdot=omega0^2*ksi^2*exp(-omega0*ksi*t).*(C1*sin(omega0*(1-ksi^2)^(1/2)*t)+C2*cos(omega0*(1-ksi^2)^(1/2)*t))-2*omega0*ksi*exp(-omega0*ksi*t).*(C1*cos(omega0*(1-ksi^2)^(1/2)*t)*omega0*(1-ksi^2)^(1/2)-C2*sin(omega0*(1-ksi^2)^(1/2)*t)*omega0*(1-ksi^2)^(1/2))+exp(-omega0*ksi*t).*(-C1*sin(omega0*(1-ksi^2)^(1/2)*t)*omega0^2*(1-ksi^2)-C2*cos(omega0*(1-ksi^2)^(1/2)*t)*omega0^2*(1-ksi^2))+omega0^2*ksi^2*exp(omega0*ksi*t).*(C3*sin(omega0*(1-ksi^2)^(1/2)*t)+C4*cos(omega0*(1-ksi^2)^(1/2)*t))+2*omega0*ksi*exp(omega0*ksi*t).*(C3*cos(omega0*(1-ksi^2)^(1/2)*t)*omega0*(1-ksi^2)^(1/2)-C4*sin(omega0*(1-ksi^2)^(1/2)*t)*omega0*(1-ksi^2)^(1/2))+exp(omega0*ksi*t).*(-C3*sin(omega0*(1-ksi^2)^(1/2)*t)*omega0^2*(1-ksi^2)-C4*cos(omega0*(1-ksi^2)^(1/2)*t)*omega0^2*(1-ksi^2));
```



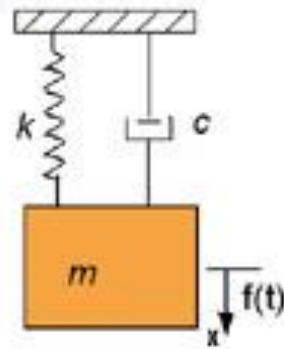
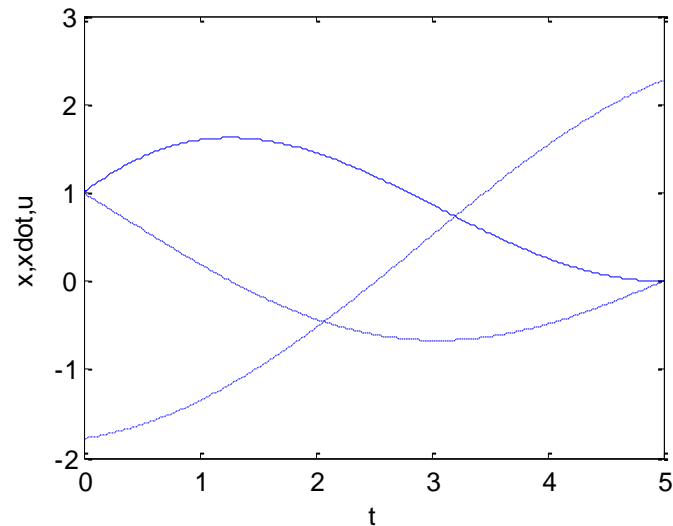
# Wyznaczenie sterowania

$$u(t) = (\ddot{x} + 2\xi\omega_0\dot{x} + \omega_0^2x) / \omega_0^2.$$

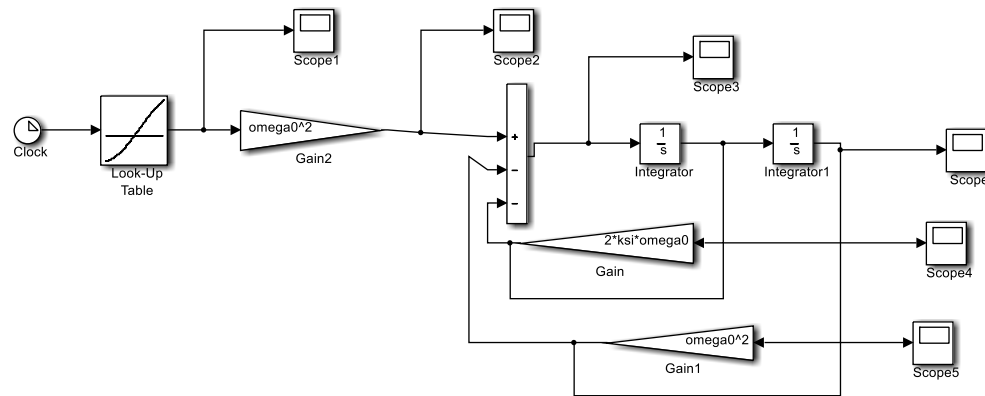
$$\omega_0 = 0,5$$

$$\xi = 0,1$$

```
u=(xdothdot+2*ksi*omega0*xdot+omega0^2*x)/omega0^2;  
plot(t,x)  
hold on  
plot(t,xdot,'--')  
hold on  
plot(t,u,'-.')  
xlabel('t'), ylabel('x,xdot,u')
```



# Symulacja



sprezynaKsiOmegaSterowanie.slx

# Sterowanie optymalne

